

Multi-date correlation of Terrestrial Laser Scanning data for the characterization of landslide kinematics

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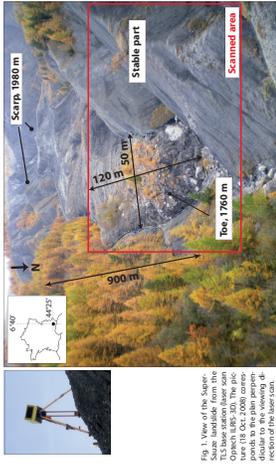


Fig. 1. View of the Super-Sauze landslide from the top. The stable part (red box) is 180 m x 120 m. The scanned area (blue box) is 1760 m x 900 m. The point cloud is derived from the TLS point cloud of the stable part of the landslide.

Objective

This work presents a simple method to characterize the 3D displacement field of landslide by exploiting all geometrical information contained in 3D point clouds with a normalized cross correlation function. The toe of the Super-Sauze landslide (South French Alps) is chosen as an experimental site (Fig. 1). The landslide extends over a distance of 900 m between an elevation of 1980 m at the crown and 1760 m at the toe with an average width of 135 m and a average slope of 25° (Malet et al., 2002).

Acquisition of TLS data

The monitoring has been realized with a long-range terrestrial laser scan Optech IL-RIS-3D (Fig. 1). Ten acquisitions were acquired between October 2007 and May 2010 for the same base station at an average distance of 100 m from the landslide. The point clouds are constituted of 9 to 12 millions of points distributed on a surface of 6'000 m² (average point density of 230 pt.m⁻²).

Co-registration and georeferencing

Each TLS dataset is aligned with a 3D error of 4 cm on the stable parts surrounding the landslide. For the georeferencing, an Airborne Laser Scanning (ALS) point cloud was used as a reference (Fig. 2). The georeferencing accuracy presents an average error of 11 cm and a standard deviation of 14 cm.

Fig. 2. Alignment of the stable parts of the different TLS point clouds on the ALS point cloud with the different coordinate systems involved in the process.

Simplification of the 3D matching problem

A projective transformation allows to represent the entire geometrical information in a plan perpendicular to the viewing direction of the scan. The relationship among the 3D position (X, Y, Z) of each point in the ground reference system to its position (u, v) in the plane reference system is given by the collinearity equations (Kraus and Waldhauser, 1994) (Fig. 2). A scaling factor is used to adjust the average point density to 1 pt.pixel⁻¹ to preserve the geometrical information. The 2D gradient of the distance between the point clouds and the TLS station is calculated for emphasizing the morphology of the landslide. The generated images are then converted in grey-scale values (Fig. 3).

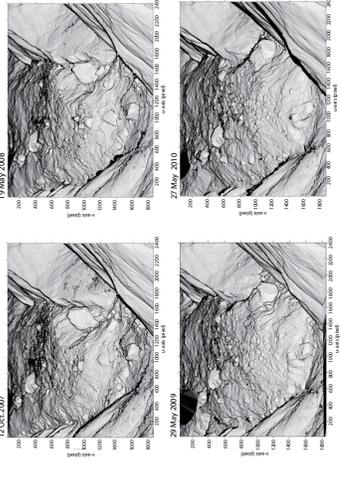


Fig. 3. Images derived from the gradient calculation on the TLS point cloud at different dates.

Determination of the displacement field by image correlation

The image correlation principle consists in recognizing identical intensity distribution patterns in a correlation window over two images to determine the displacement of the center of the window by maximizing a normalized cross correlation function (Lewis, 1995).

The result of the correlation corresponds to the displacements Δu and Δv along the u-axis and v-axis. To reconstruct the 3D displacement field, a triplet of coordinates (X, Y, Z) obtained from the first and the second TLS acquisitions is associated to each initial (u, v) and final position (u+ Δu , v+ Δv) of the displacement vectors in the images. The median of the displacement components (ΔX , ΔY , ΔZ) located in the same mesh (one-meter grid mesh size) is then computed.

Strain computation

A strain analysis is applied to characterize possible different behaviours in the landslide material. A local least square fitting technique is used to compute the Cauchy's strain tensor **E** at each location of the grid (Pan et al., 2009). The two eigenvalues ϵ_1 and ϵ_2 of **E** corresponding to the change of length per unit length in the direction having the maximum and minimum extension (positive for extension without shearing are computed). The deformation is presented by the surface strain defined as $\epsilon_s = \epsilon_1 + \epsilon_2$ (positive for extension) and the shear strain defined as $\gamma = |\epsilon_1 - \epsilon_2|$.

Kinematic analysis

For the period July-October 2008, displacements between 0.5 and 1.5 m are observed (average displacement rate of 0.6-1.7 cm.day⁻¹). The largest displacements are detected at the front of the toe (Fig. 4A). For the period July-October 2009, shorter displacements ranging from 0.1 m at the front of the landslide toe to 0.6 m in the upper part of the toe are observed (average displacement rate of 0.1-0.8 cm.day⁻¹; Fig. 4B).

In 2008 and 2009, the upper part of the toe is characterized by a succession of approximately parallel bands (width of 5 to 10 m) in compression and extension which main orientation is perpendicular to the sliding direction (Fig. 4C-D). The behavior at the front of the toe is very different for the two years. In 2008, the extension behavior creates tensile fissures and important shearing located along the landslide boundary (Fig. 4E). This confirmed by the presence of very persistent tensile and shear fissures observed in the field from very high resolution images (Fig. 5). In 2009, the deformation affecting the front toe is less important (Fig. 4F).

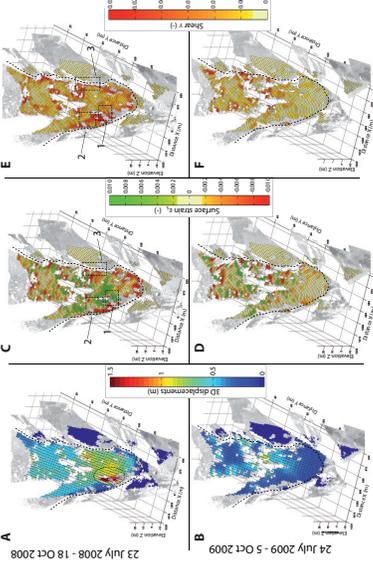


Fig. 4. Results of the displacement and strain analysis for the period July-October 2008. (A) Calculated displacement field in 2008 (m) with a distance in m. (B) Calculated displacement field in 2009 (m) with a distance in m. (C) Calculated surface strain (positive for extension, negative for compression). (D) Calculated shear strain. The locations 1, 2 and 3 in C and E are detailed in Fig. 5.

Validation of the computed displacements

The computed displacements are in very good agreement with the displacements obtained with the iterative Closest Point algorithm (Barnes et al., 1998) using the ground truth and standard deviation of 3 cm (Fig. 6B) and observed from the GPS monitoring of five blocks at the landslide toe (average error of 4 cm and standard deviation of 3 cm; Fig. 6A-C).

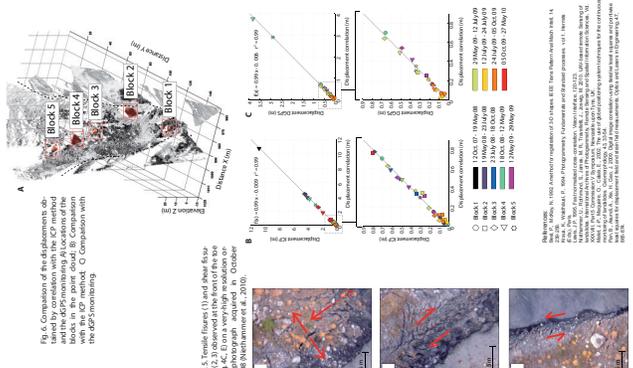
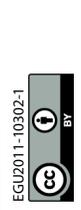


Fig. 6. Comparison of the displacement fields obtained with the iterative Closest Point algorithm and the displacement field computed with the K2P method. (A) Location of the five blocks monitored by the GPS. (B) Displacement field computed with the iterative Closest Point algorithm. (C) Displacement field computed with the K2P method. (D) Comparison of the displacement fields with the K2P method.



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