

# Single-well tracer test sensitivity w. r. to hydrofrac and matrix parameters (case study for the Horstberg site in the N-German Sedimentary Basin)

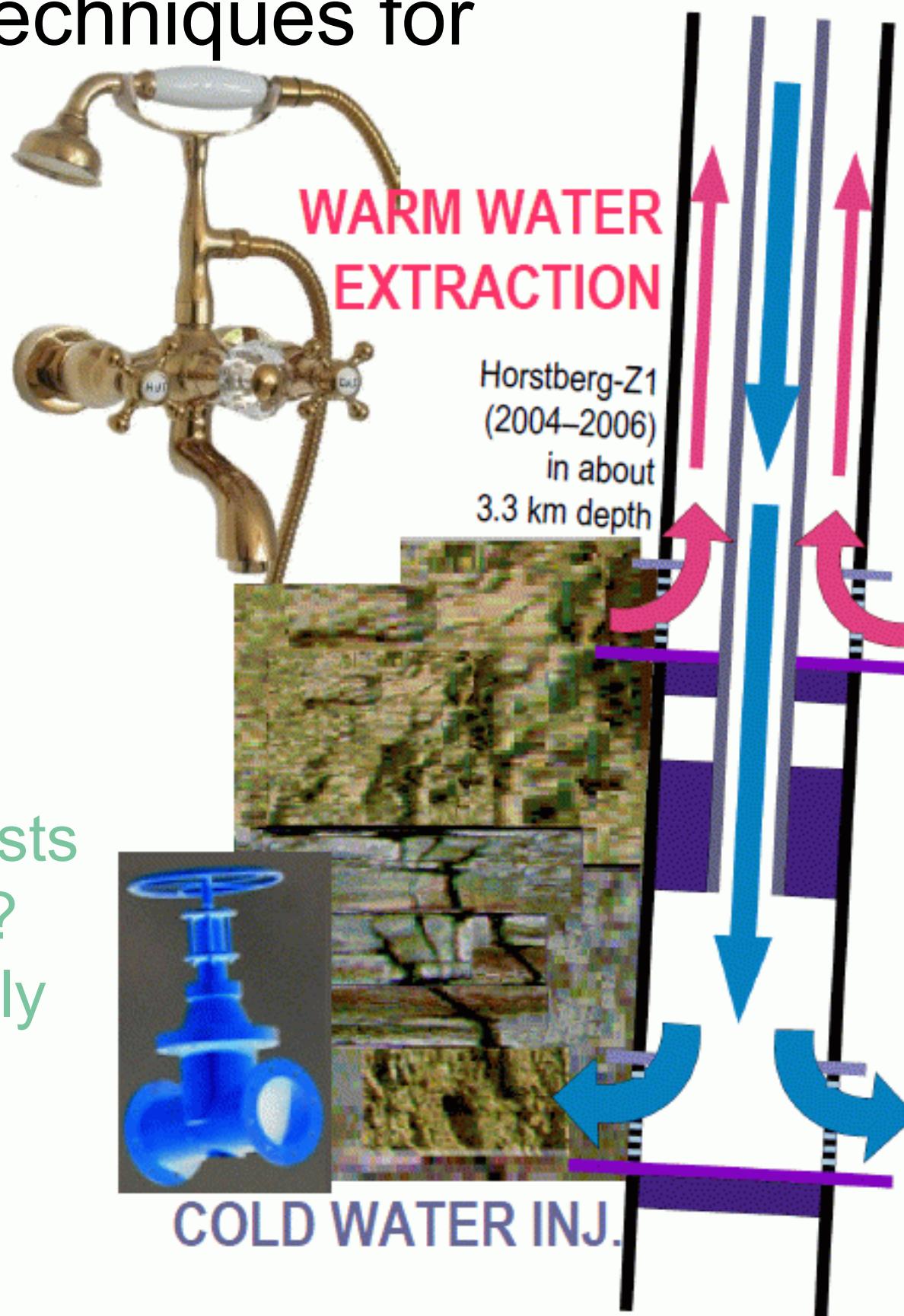
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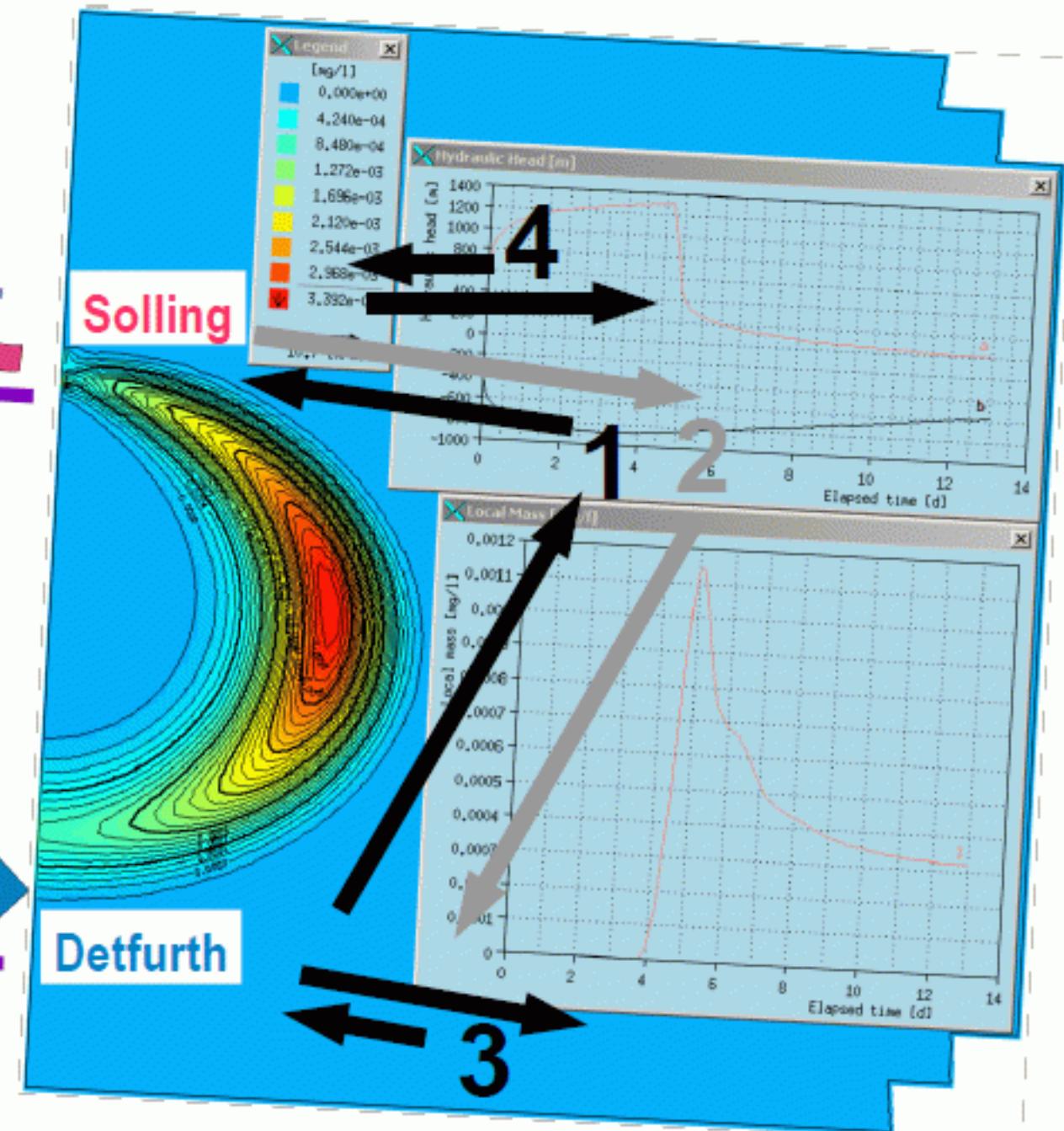


# MOTIVATION : evaluating innovative, single-well techniques for geothermal heat extraction from deep tight (lowly permeable) rock

what kind of tests  
– make sense?  
– are technically feasible?



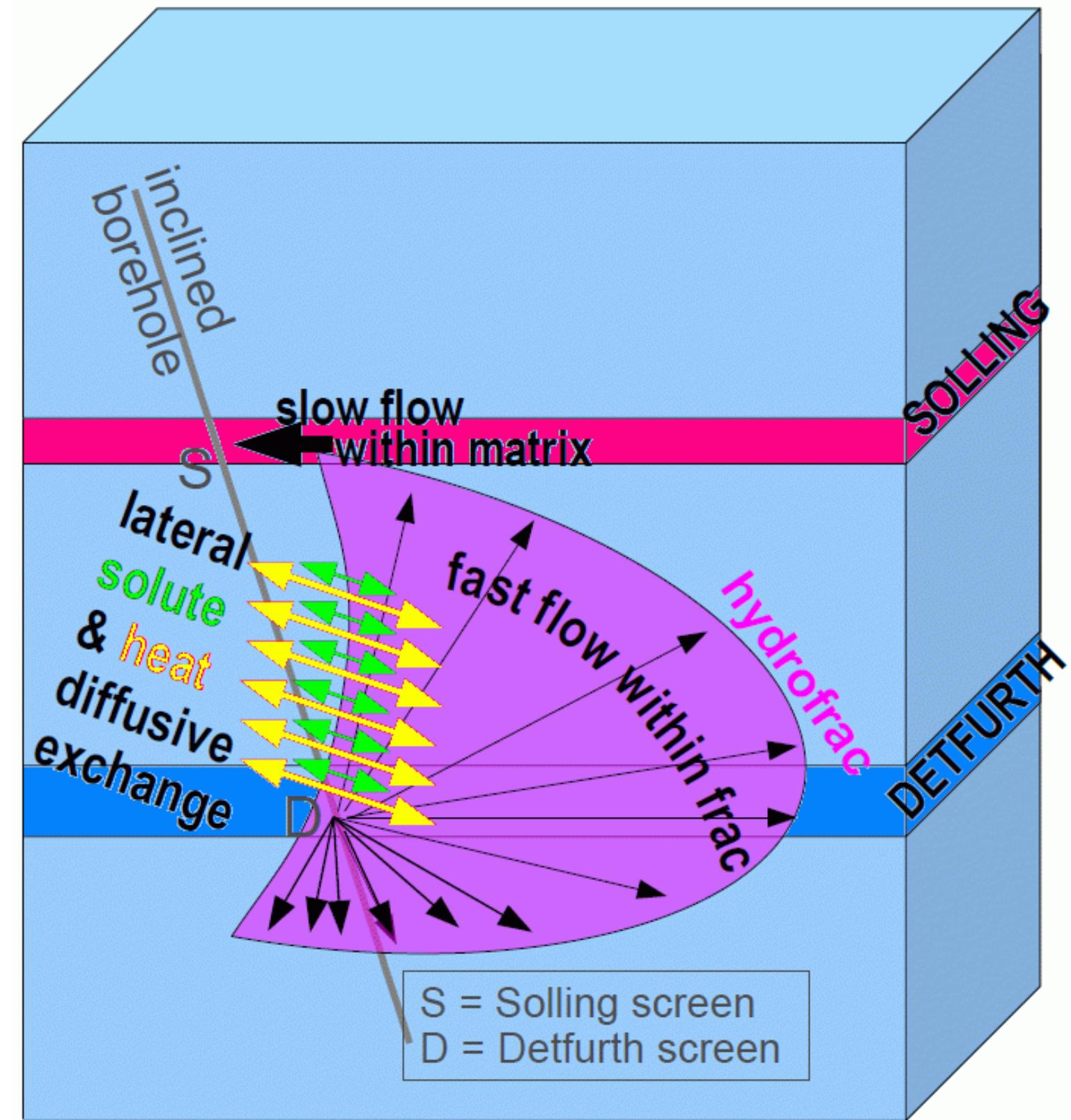
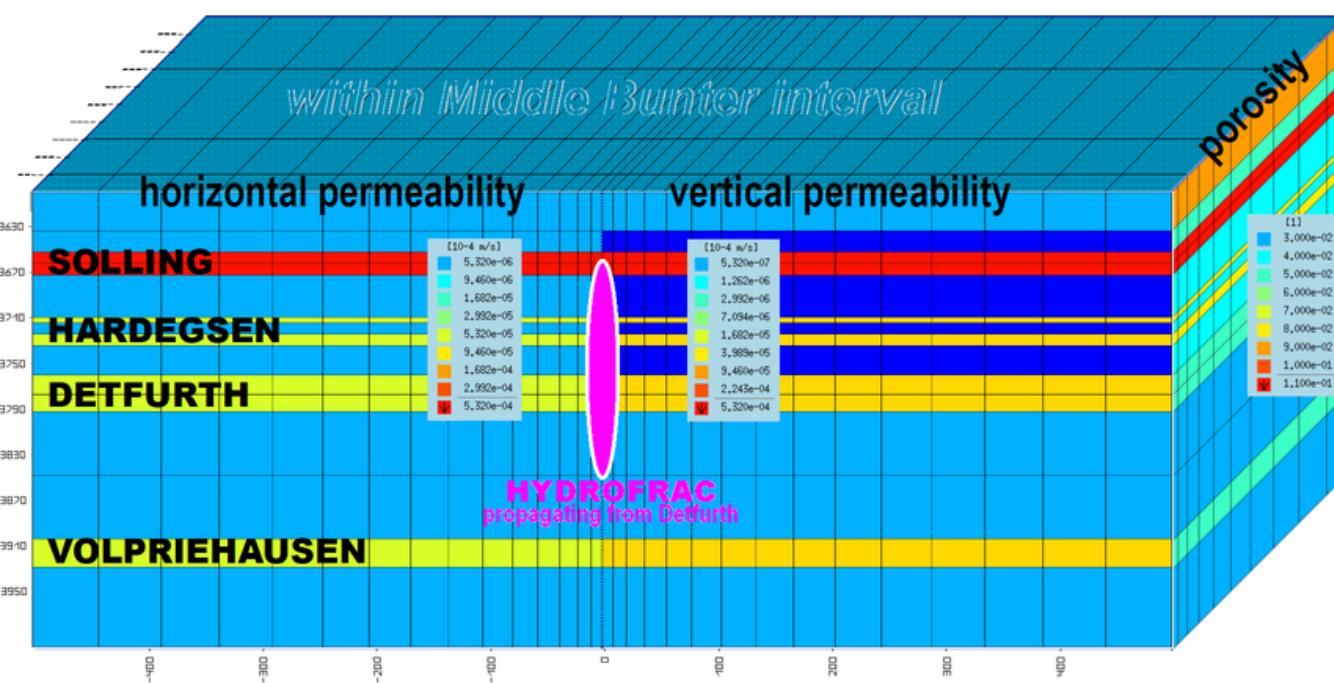
- flow-path tracing ( 1 , 2 )
- tracer push-pull tests ( 3 , 4 )



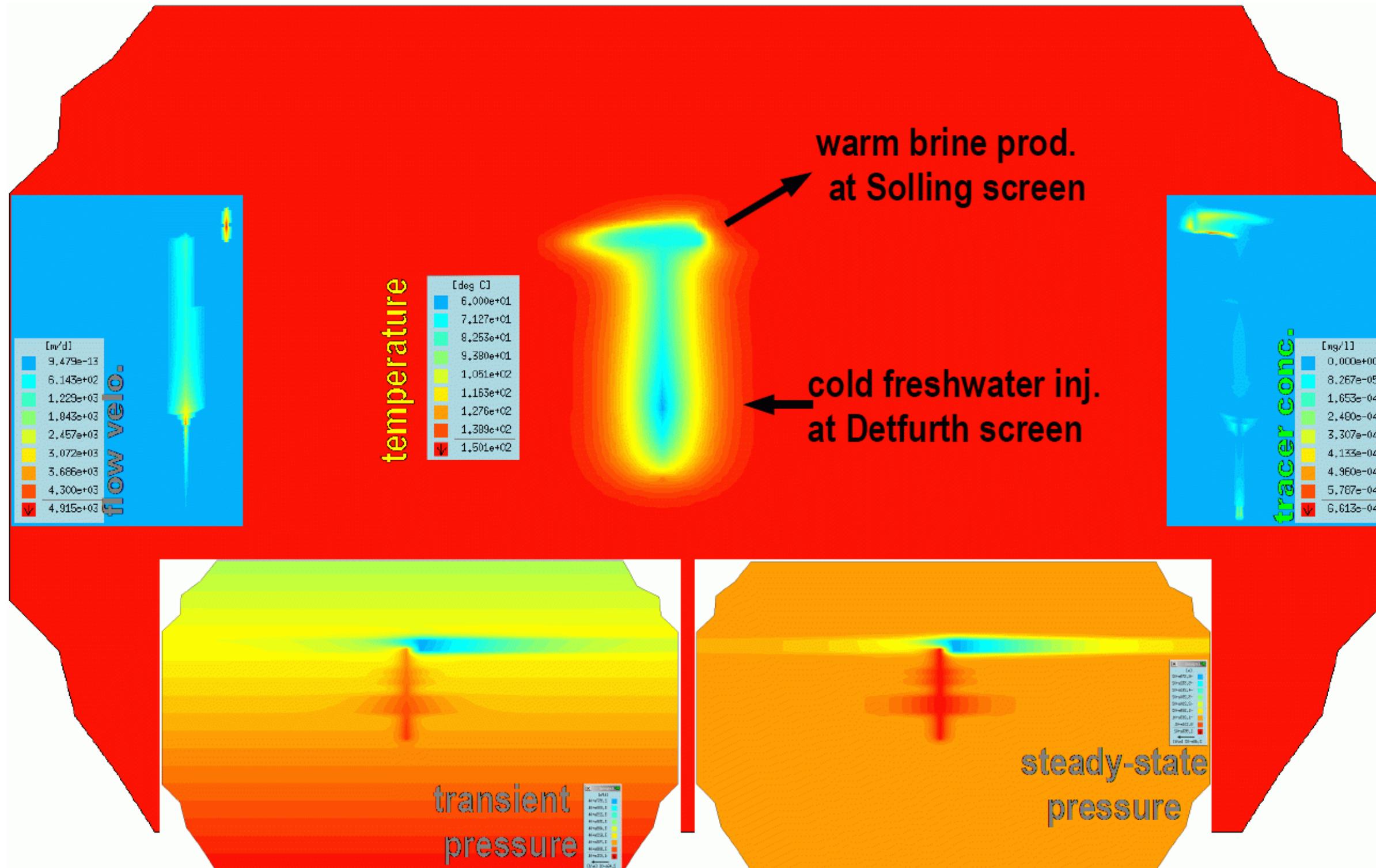
# PROCESSES

- rapid flow (Hagen-Poiseuille) within frac
- slow flow (Darcy) within matrix
- advection-dispersion within frac
- diffusion-dominated transport within matrix
- diffusive exchange ('matrix diffusion') of heat and solute (tracer)  $\text{frac} \leftrightarrow \text{matrix}$

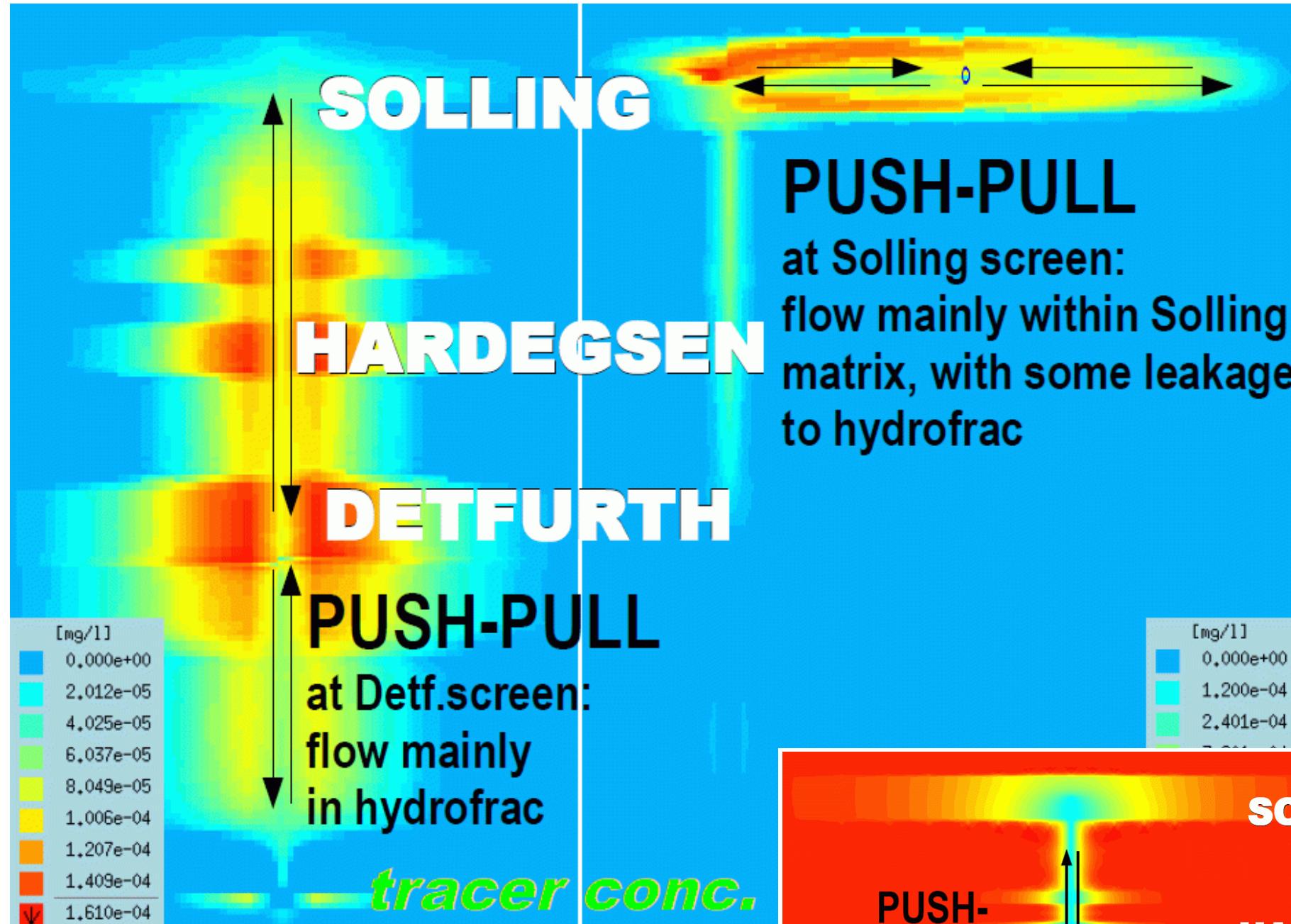
## MODEL PARAMETRIZATION



# INTER-LAYER TEST (1)

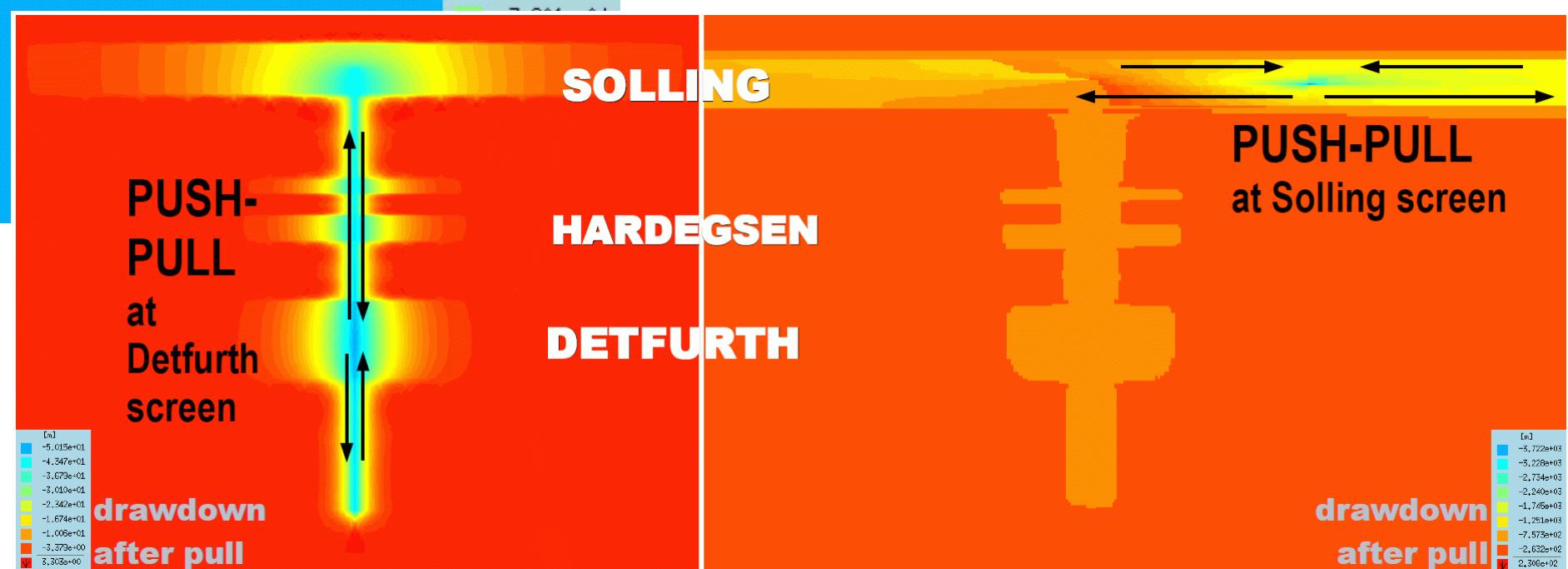


# SINGLE-LAYER TESTS (3,4)



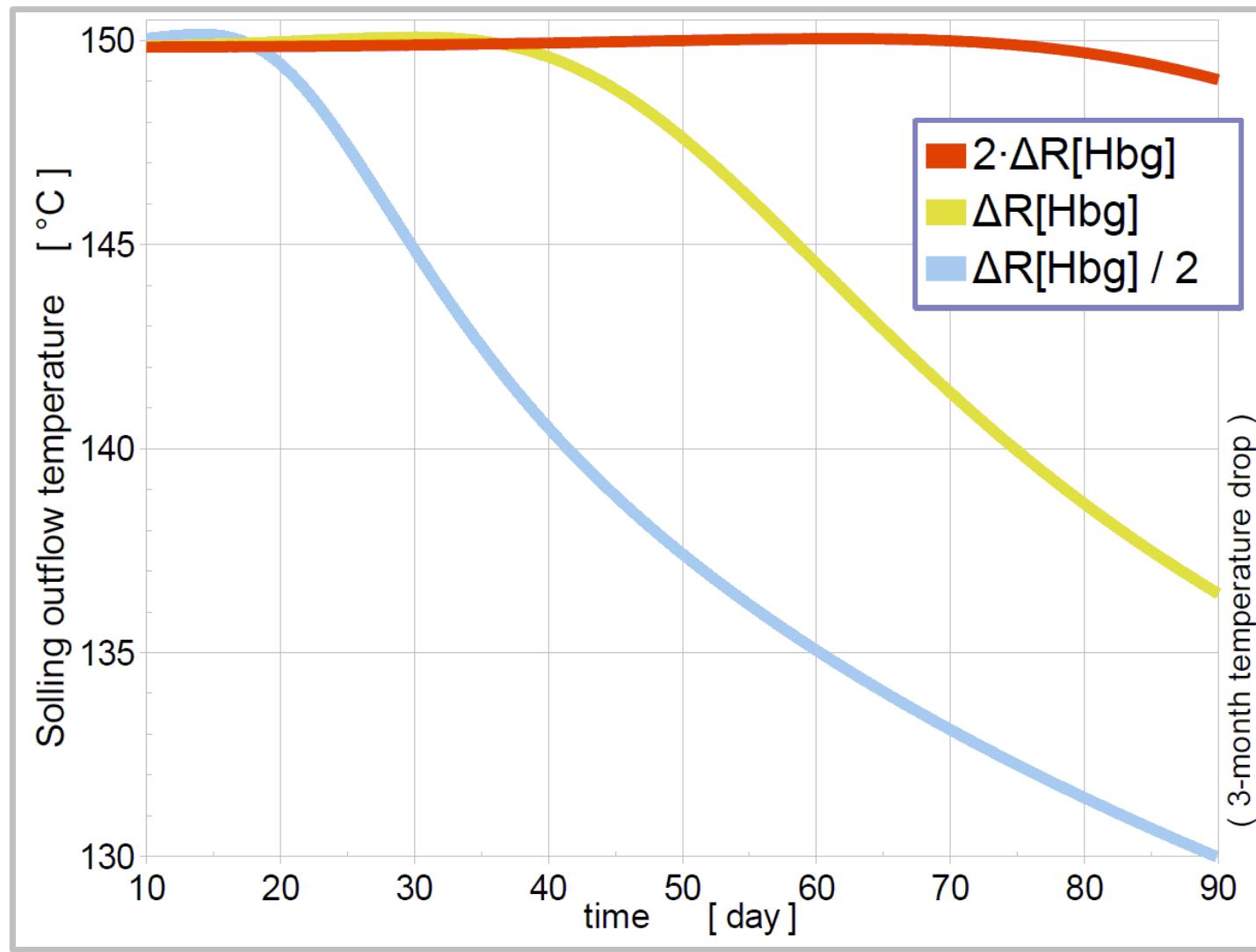
tracer push-pull tests

- at Dettfurth screen:
  - insensitive w.r.to matrix parameters
  - ambiguously sensitive w.r. to frac aperture
- at Solling screen:
  - sensitive w.r.to matrix parameters
  - limited sensitivity w.r.to frac parameters

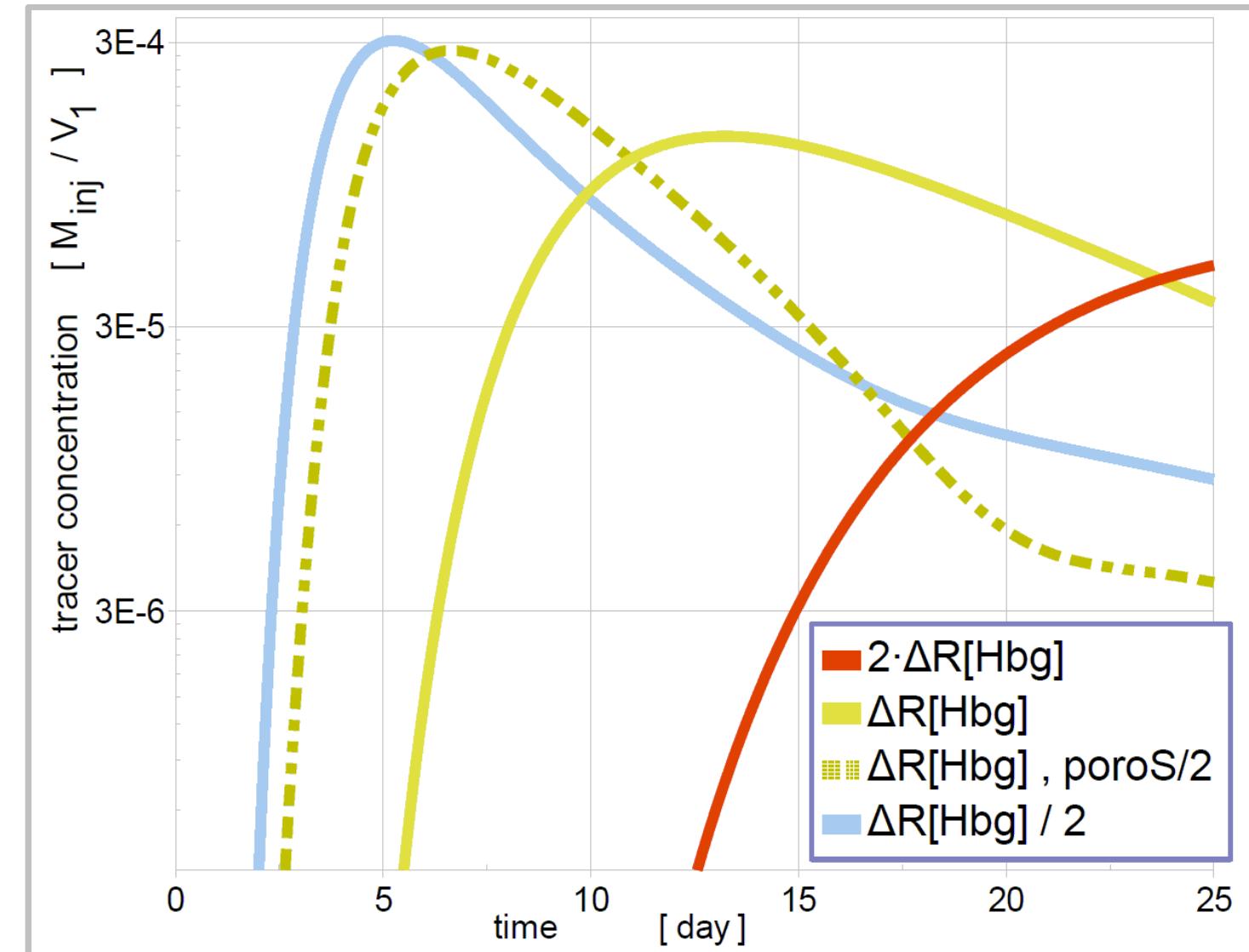


# HEAT – TRACER CORRELATION

Which parameters determine the system's thermal lifetime?



Which parameters can be determined from tracer tests?



# PARAMETER SENSITIVITY (summary)

PARAMETER controlling for ...? invertible from...?	... thermal lifetime?	... tracer signal from inter-/single-screen experiment?		
	1 , 2	3	4	
frac dist. ( $\Delta R$ ) from Solling screen	yes : via <b>MRT</b>	yes; <b>mT</b>	no	only with large PUSH volume; <b><math>m\infty</math></b>
frac length ( $L_2$ ) at Solling bottom	yes : via <b>HEA</b>	yes; <b>mT</b> , <b><math>m\infty</math></b>		
frac aperture ( $b$ , dynamical)	no		with restrictions; <b><math>mX</math></b>	
Solling porosity ( $\omega$ )	weak influence via <b>MRT</b>	yes; <b>mT</b>	no	only indirectly, via Pelet no. PE (not really quantifiable)
Solling fissure density ( $1/a$ )	only at low fissure density ambiguous via <b>HEA</b>	yes; <b><math>m\infty</math></b>		generally yes; a non-trivial task
	<b>MRT</b> = mean residence time <b>HEA</b> = heat exchange area	<b>mT</b> : multiple residence-time inversion <b><math>m\infty</math></b> : multiple (PULL) tailing inversion <b><math>mX</math></b> : multiple PULL (peak) inversion		
reason for <b>mT</b> :	<b>MRT</b> (1,2) $\leftarrow$ product ( $\omega \times L_2 \times \Delta R$ ), individual factors not uniquely determinable			
reason for <b><math>m\infty</math></b> :	tailing (1,2) increases with ( $1/a$ ) as well as with $L_2$ PULL tailing (4) results from $\geq 5$ mutually-independent parameters			
reason for <b><math>mX</math></b> :	PULL signal (3) relates uniquely with $b$ only above a certain PE-threshold (not likely to be reached within frac flow)			

# FOR COMPARISON :

*Same test type, conducted at different wellbore screens or different reservoir life stages, yields different parameters:*

Tracing Design	Where	When	Which parameters best determined?	
single-well	flow-path Horstberg	Detfurth → Solling clay layers + sandst.	reservoir creation early post-frac stage	frac distance from prod. wellscreen
		Detfurth sandst.		frac aperture
	Solling sandst.		reservoir operation	matrix rock-fluid interface area
inter-well	Gross Schönebeck	selected sandst. or volc. intervals	reservoir creation early post-frac stage	frac size
		sandstone and volcanics layers	reservoir operation	fluid resid.time