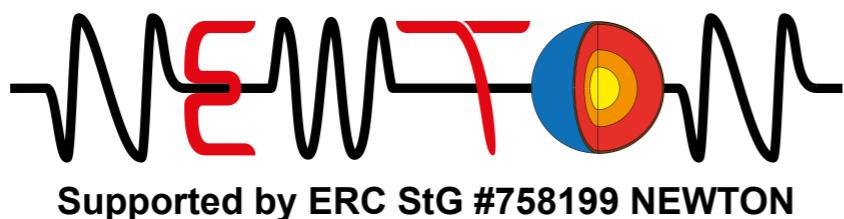




# EXTRINSIC VISCOUS ANISOTROPY OF NEWTONIAN TWO-PHASE AGGREGATES, FABRIC PARAMETRISATION AND APPLICATION TO MANTLE CONVECTION

**Albert de Montserrat, Manuele Faccenda**

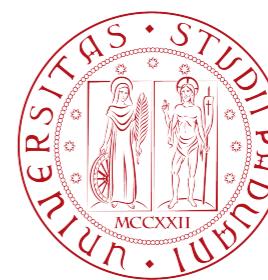
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# RATIONALE

Earth's rock formations are mechanically heterogeneous , i.e. different degrees of extrinsic mechanical anisotropy at different scales

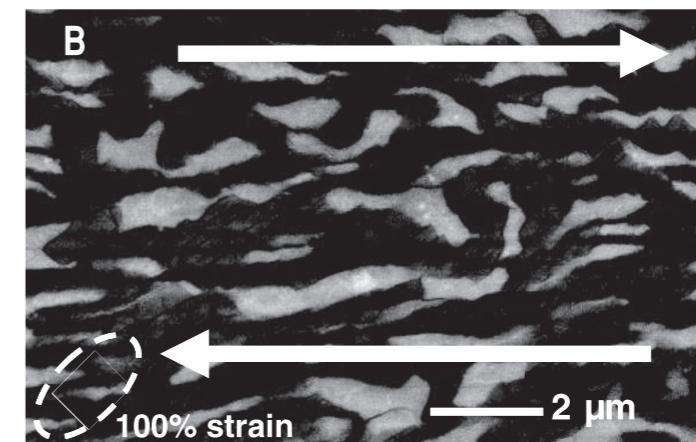
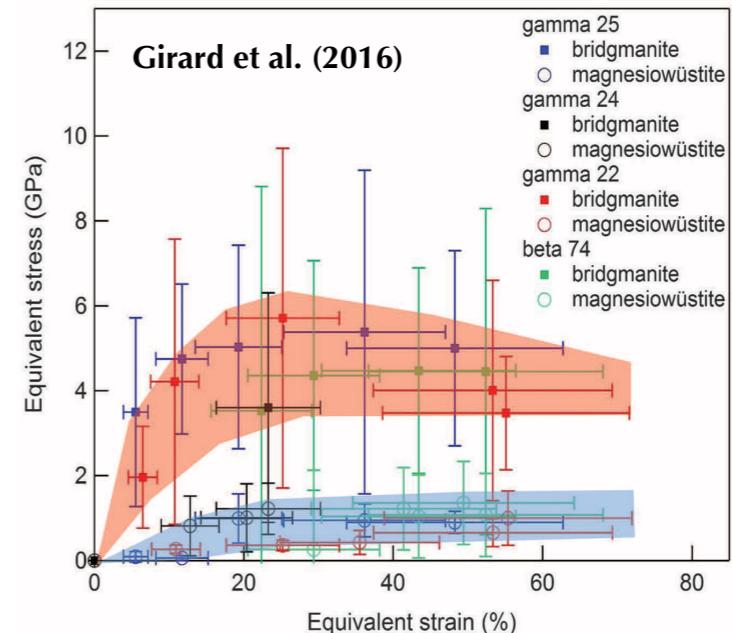
## Macro-scale



Cilindro de Marboré  
(Monte Perdido, Spain)

Folding formed by compression of a layers with distinct visco-elastic properties

## Micro-scale



The **bridgemanite/magnesiowüstite** is a lower mantle two-phase aggregate with an abundant strong phase (bridgemanite) and a sparse weak phase (magnesiowüstite)

## PROBLEM

**Large scale geodynamic models:  
anisotropy length scale << resolution**

**Only for specific shapes and non  
interactive mineral phases**

**Large scale geodynamic models:  
do not predict rock fabrics**

## SOLUTION

**Analytical solutions to predict  
anisotropic viscous/elastic tensors  
(e.g. Differential Effective Medium)**

**Average composite morphology**

**Parametrise fabric**

$$\text{Differential Effective Medium (DEM): } \frac{d\mathbb{C}_{DEM}}{d\phi} = \frac{1}{1-\phi} (\mathbb{C}_I - \mathbb{C}_{DEM}) \mathbf{A} \quad (\text{McLaughlin, 1977})$$

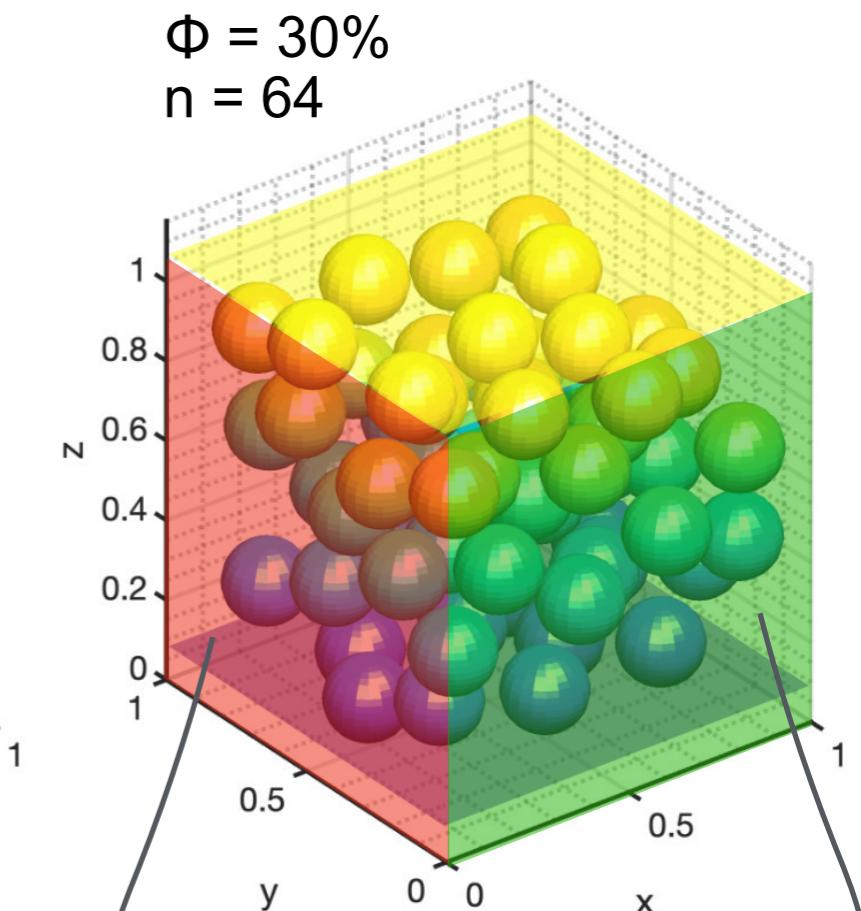
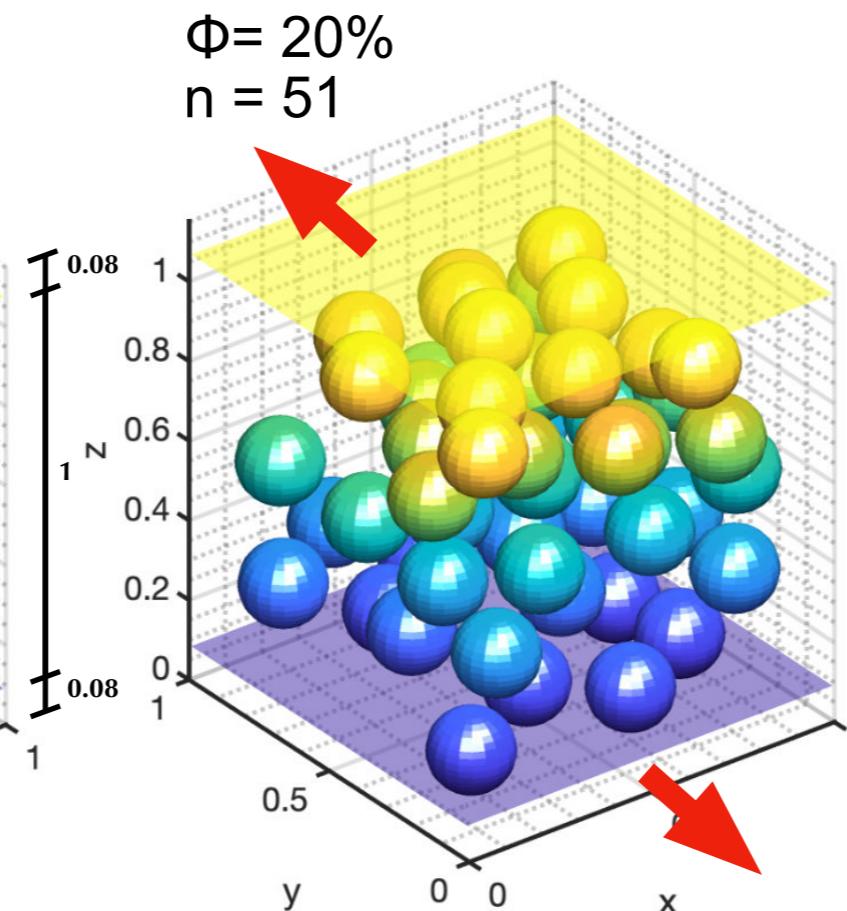
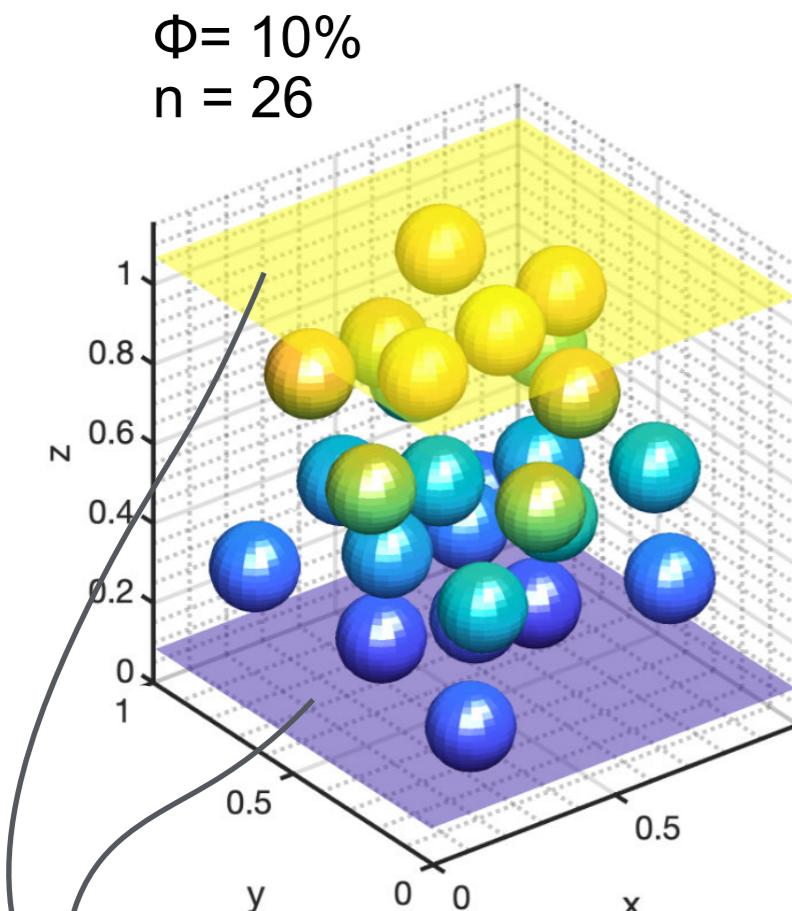
$\mathbf{A} \rightarrow$  Strain partitioning 4<sup>th</sup> order tensor     $\mathbb{C} \rightarrow$  (viscous) stiffness tensor     $\phi \rightarrow$  volume fraction

◎ Incompressible flow + Newtonian rheology

◎ Stokes equations



Finite Differences + particles in cell  
(Gerya & Yuen, 2007)



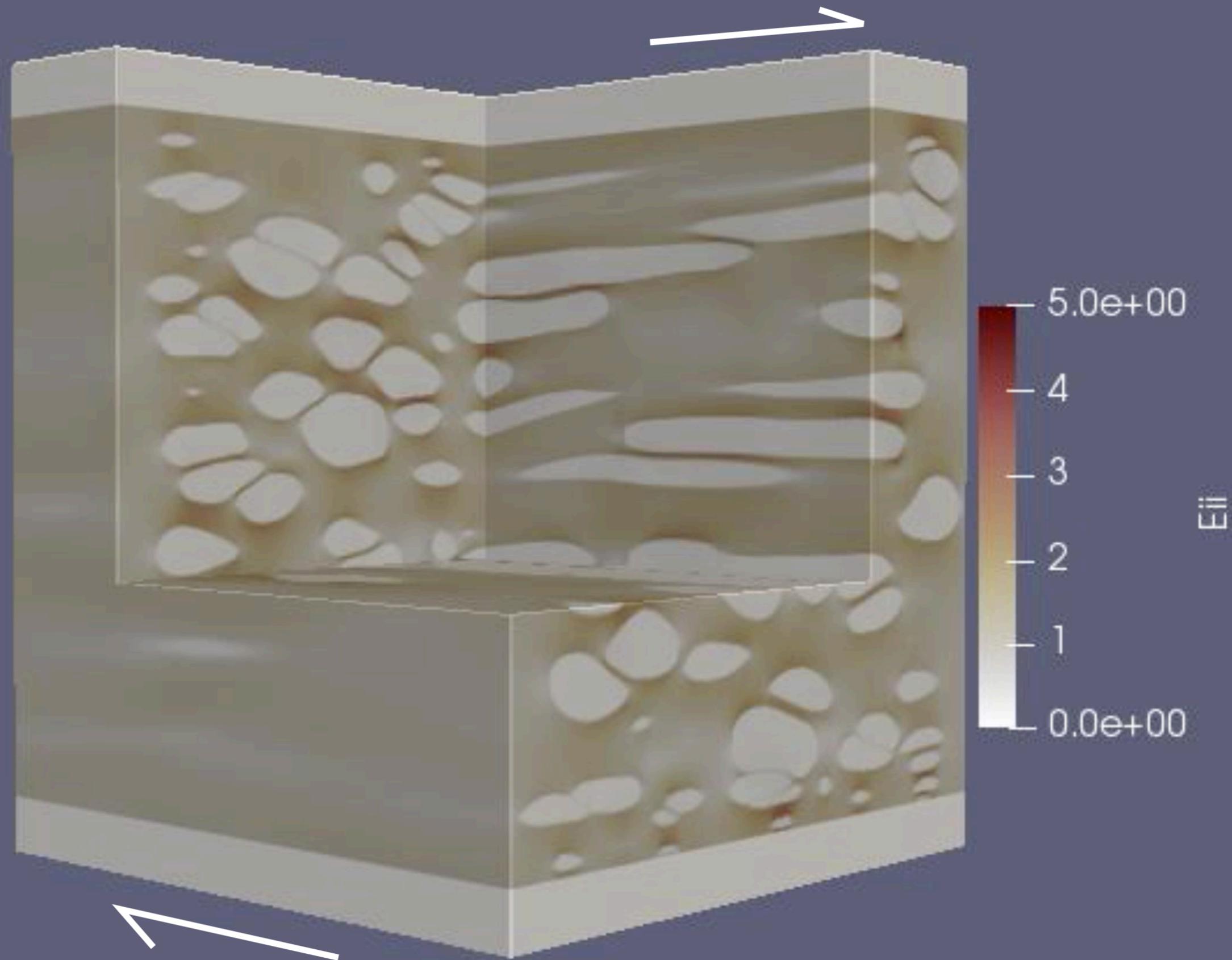
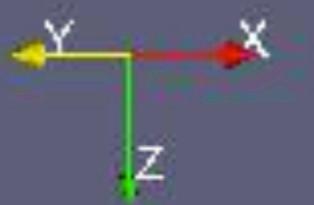
DEM vs AVERAGED FABRIC

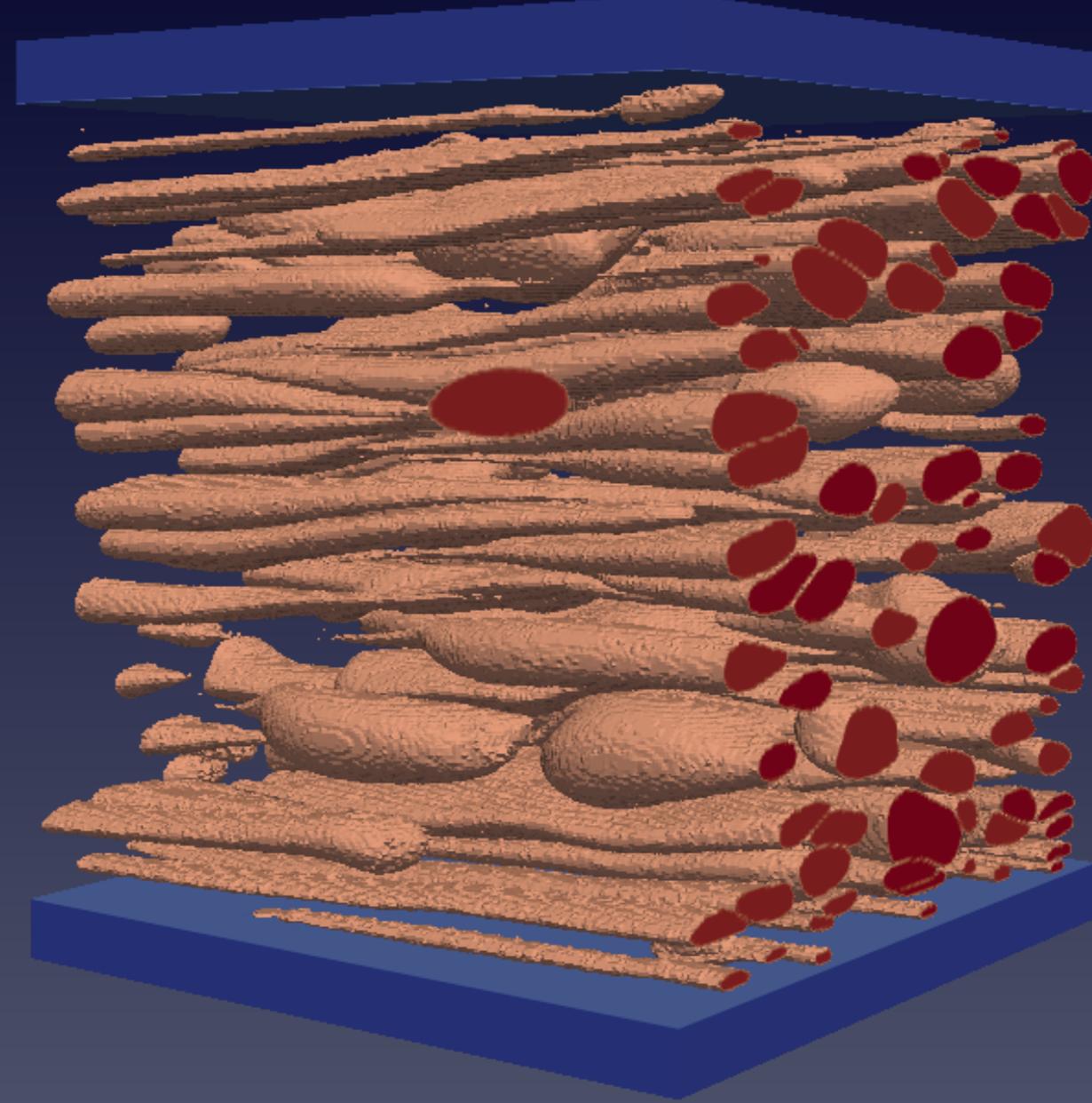
3D Models: Evolution - strong inclusions

$$\Delta\eta = 10$$

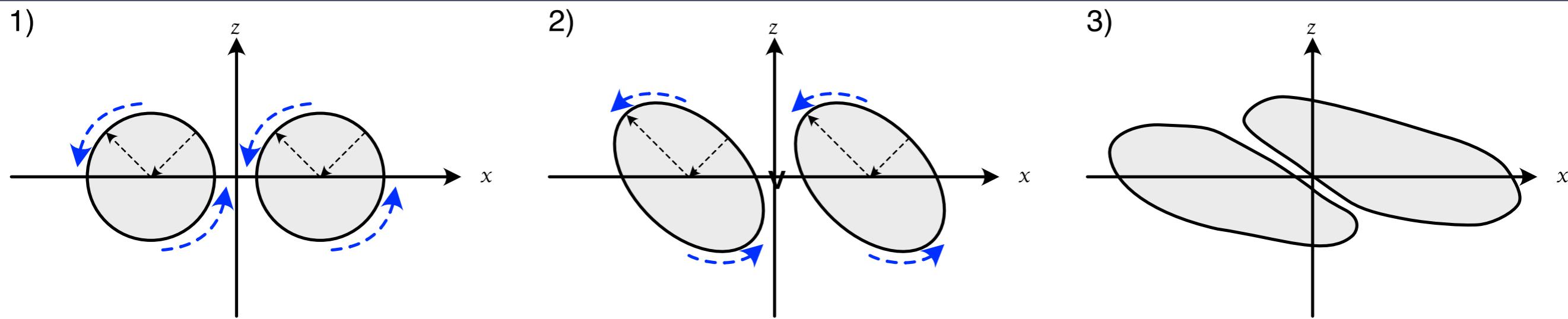
$$\phi = 30 \%$$

$$\gamma^{max} \approx 12.5 \%$$





- Tiling effect between inclusions
- Cigar-shaped inclusions



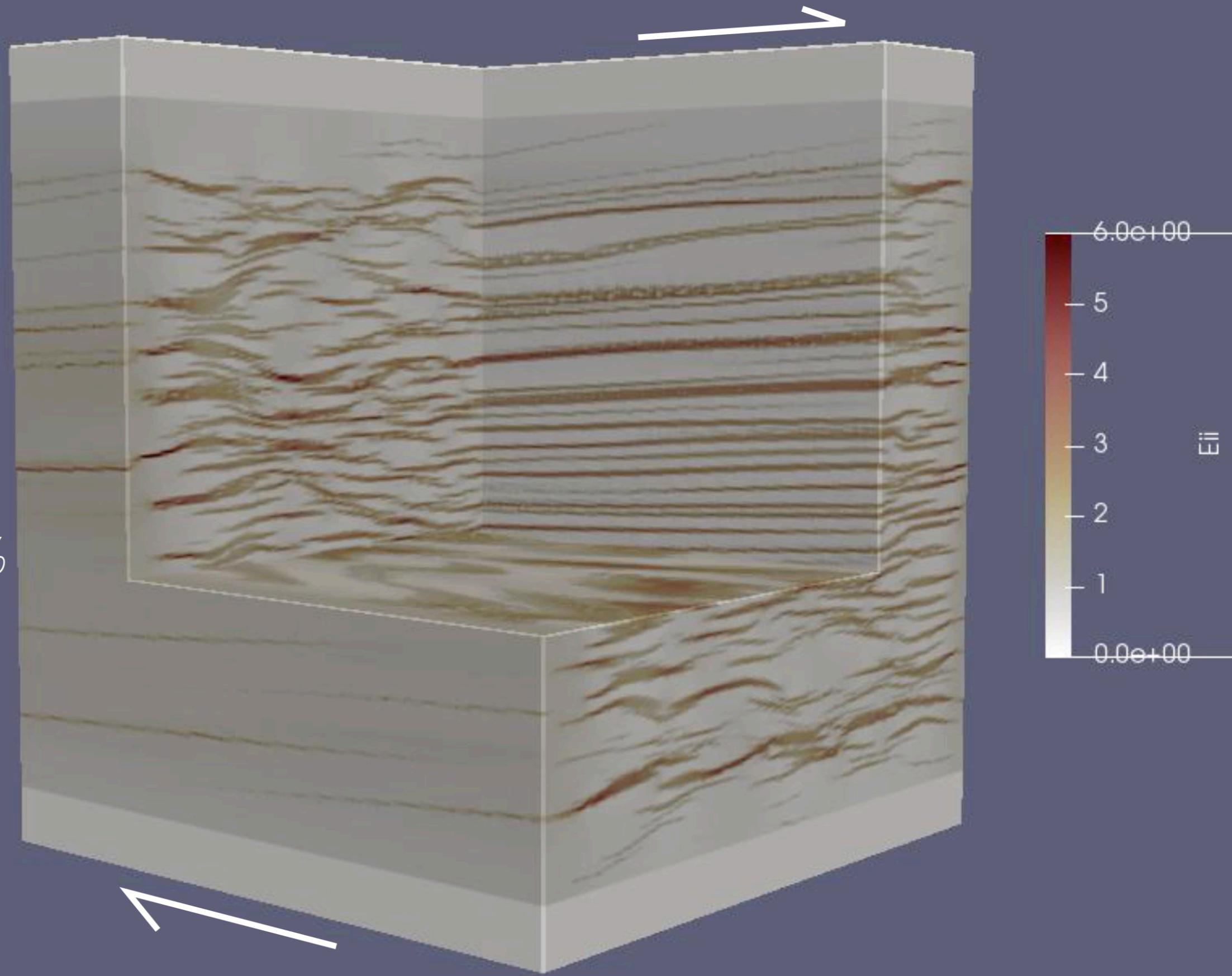
# DEM vs AVERAGED FABRIC

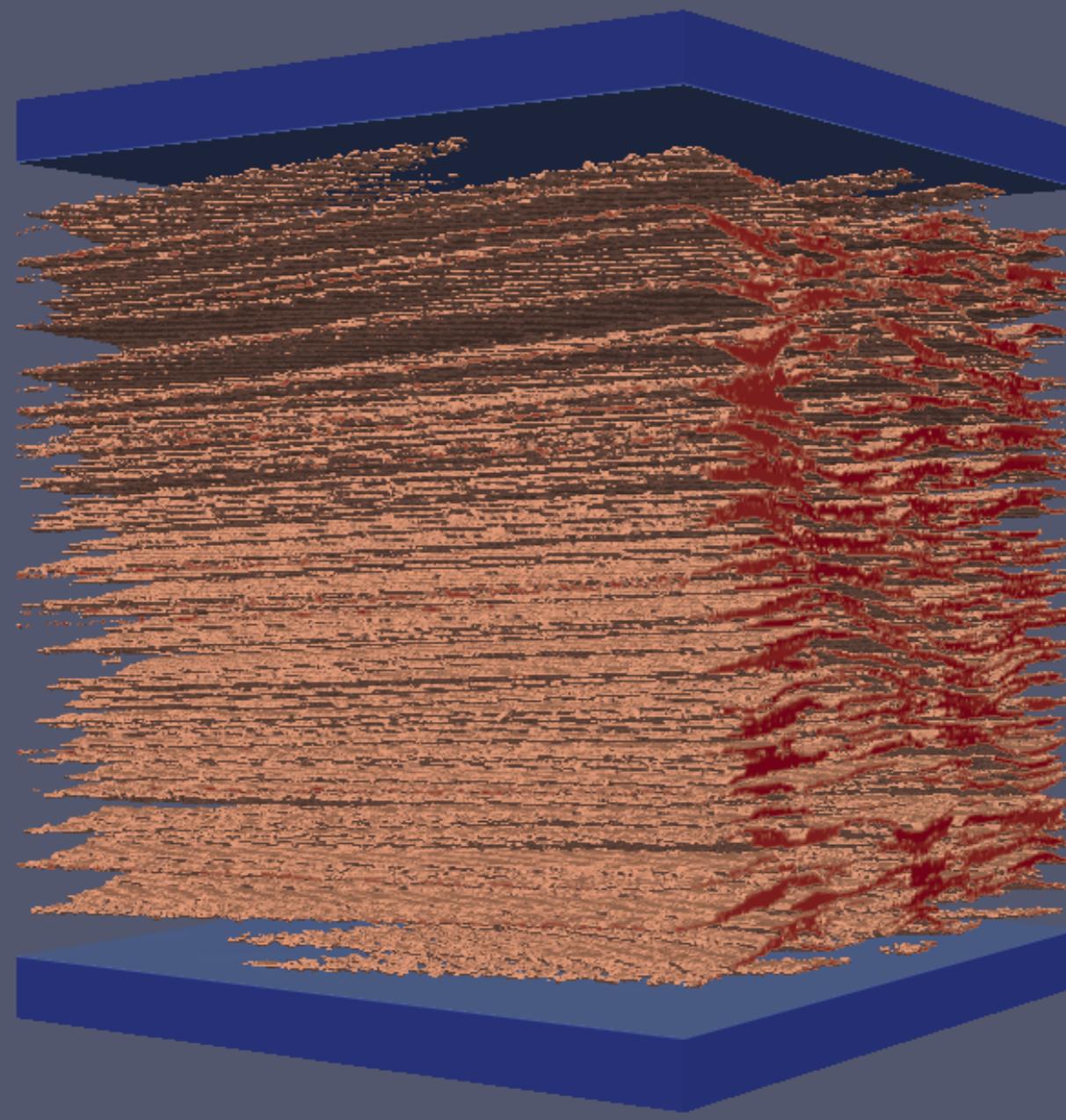
# 3D Models: Evolution - weak inclusions

$$\Delta\eta = 1/10$$

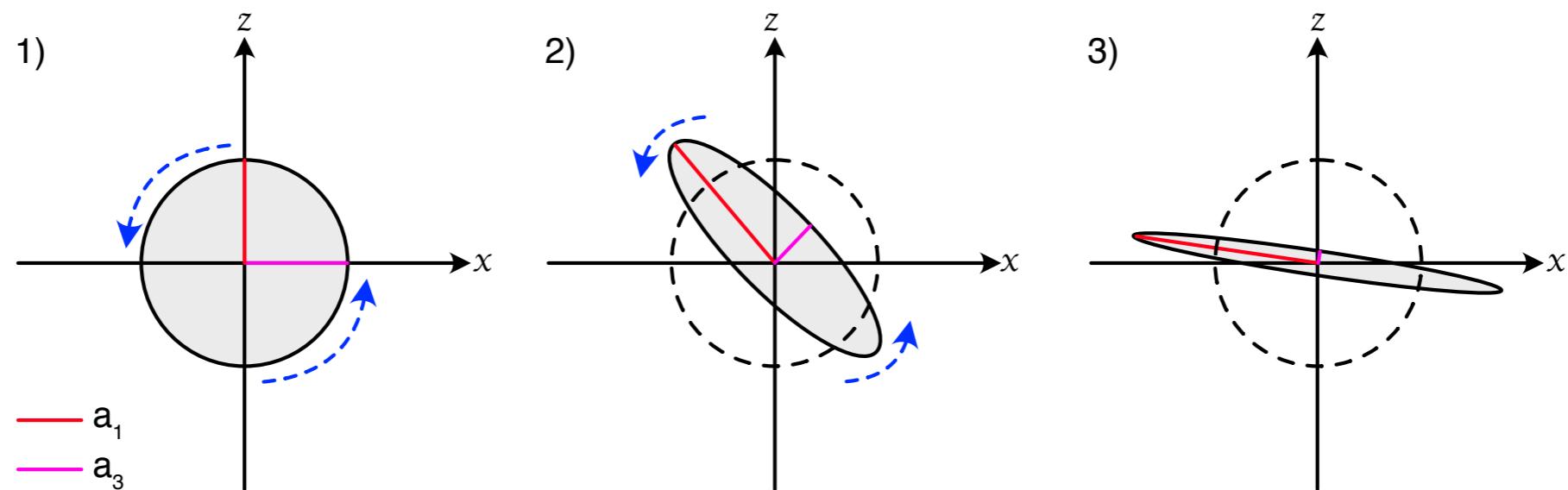
$$\phi = 30 \%$$

$$\gamma^{max} \approx 12.5 \%$$



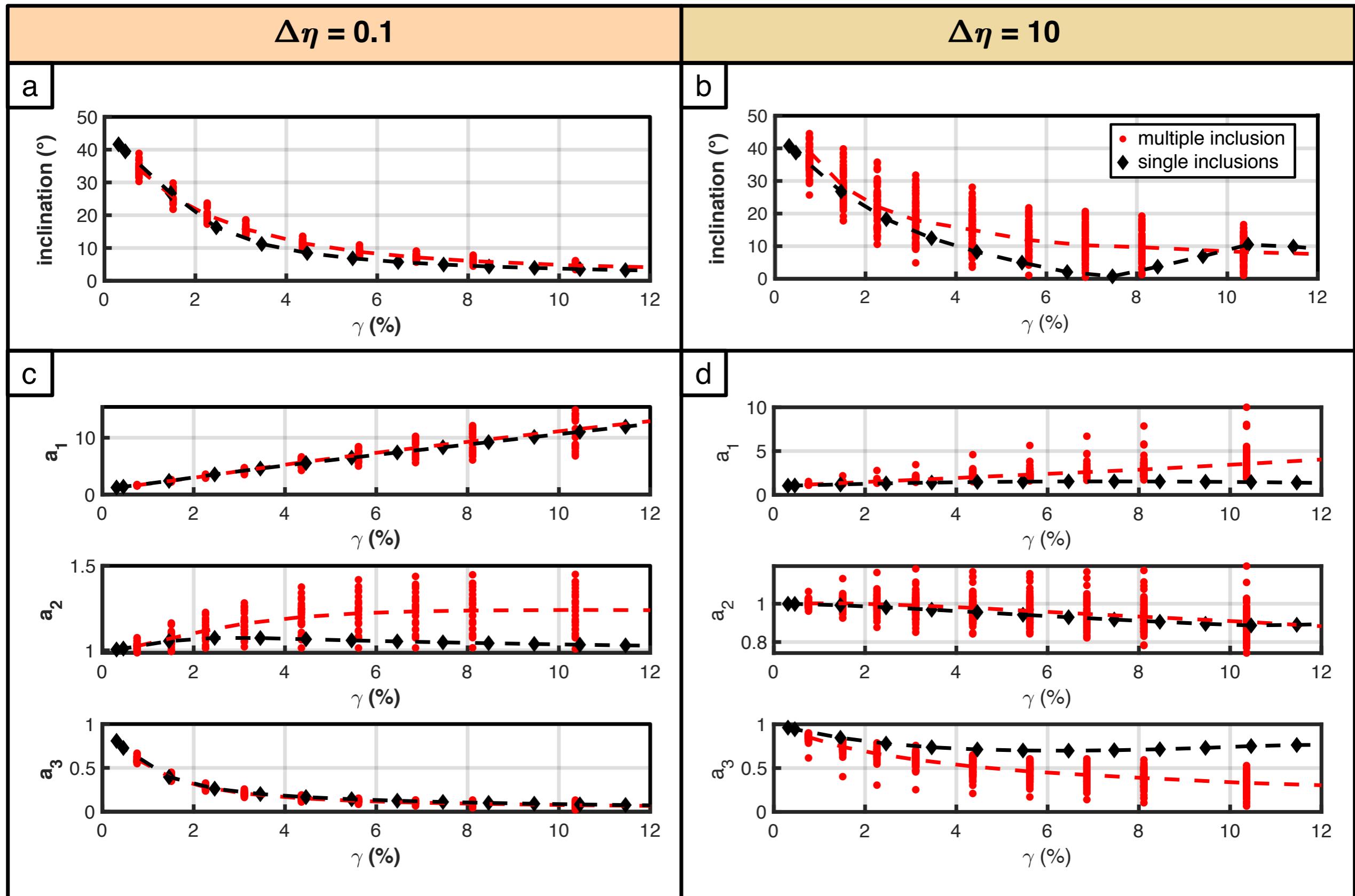


- Laminar fabric
- Boudinage



# DEM vs AVERAGED FABRIC

## Inclusion shape/inclination ( $\phi = 10\%$ )

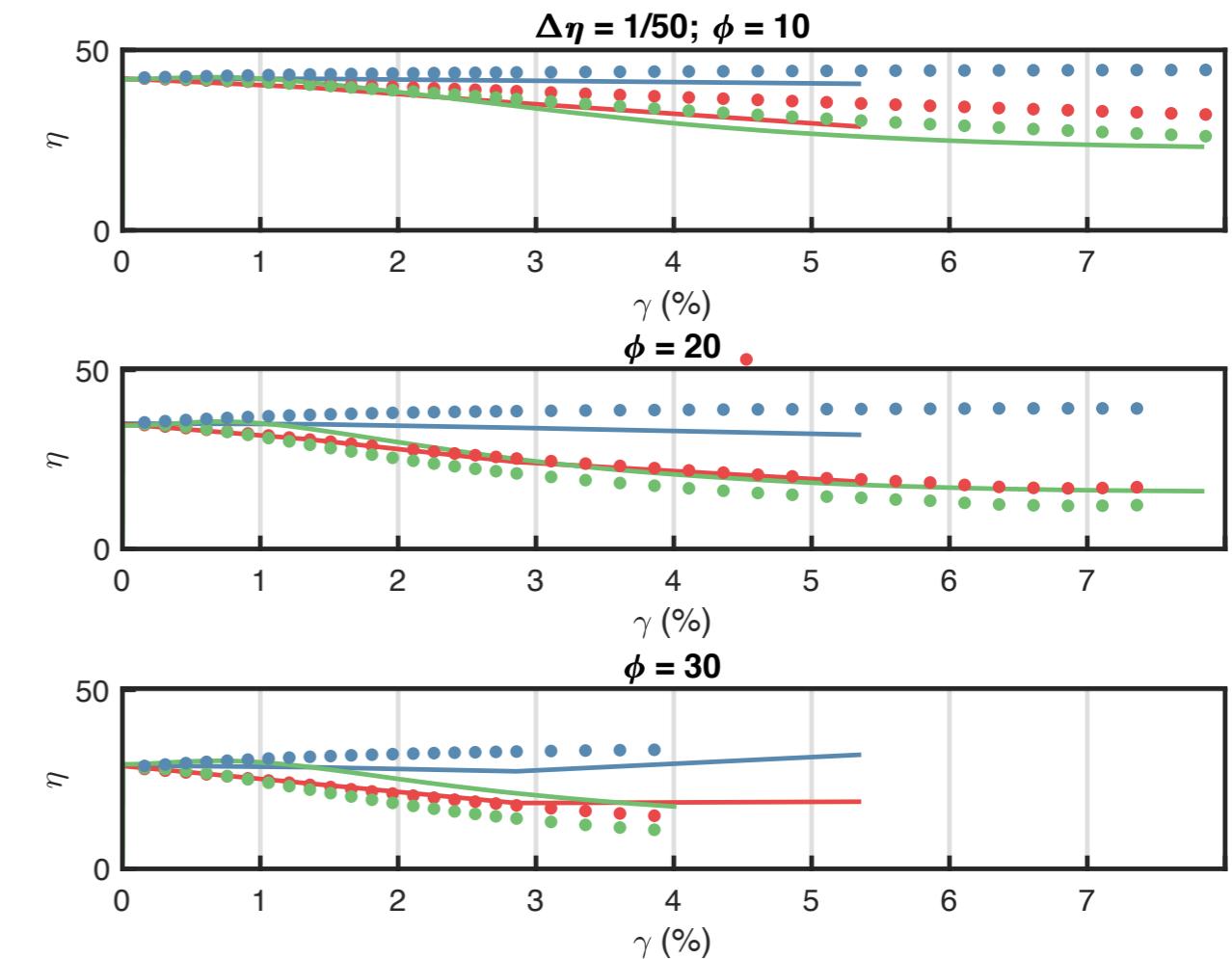
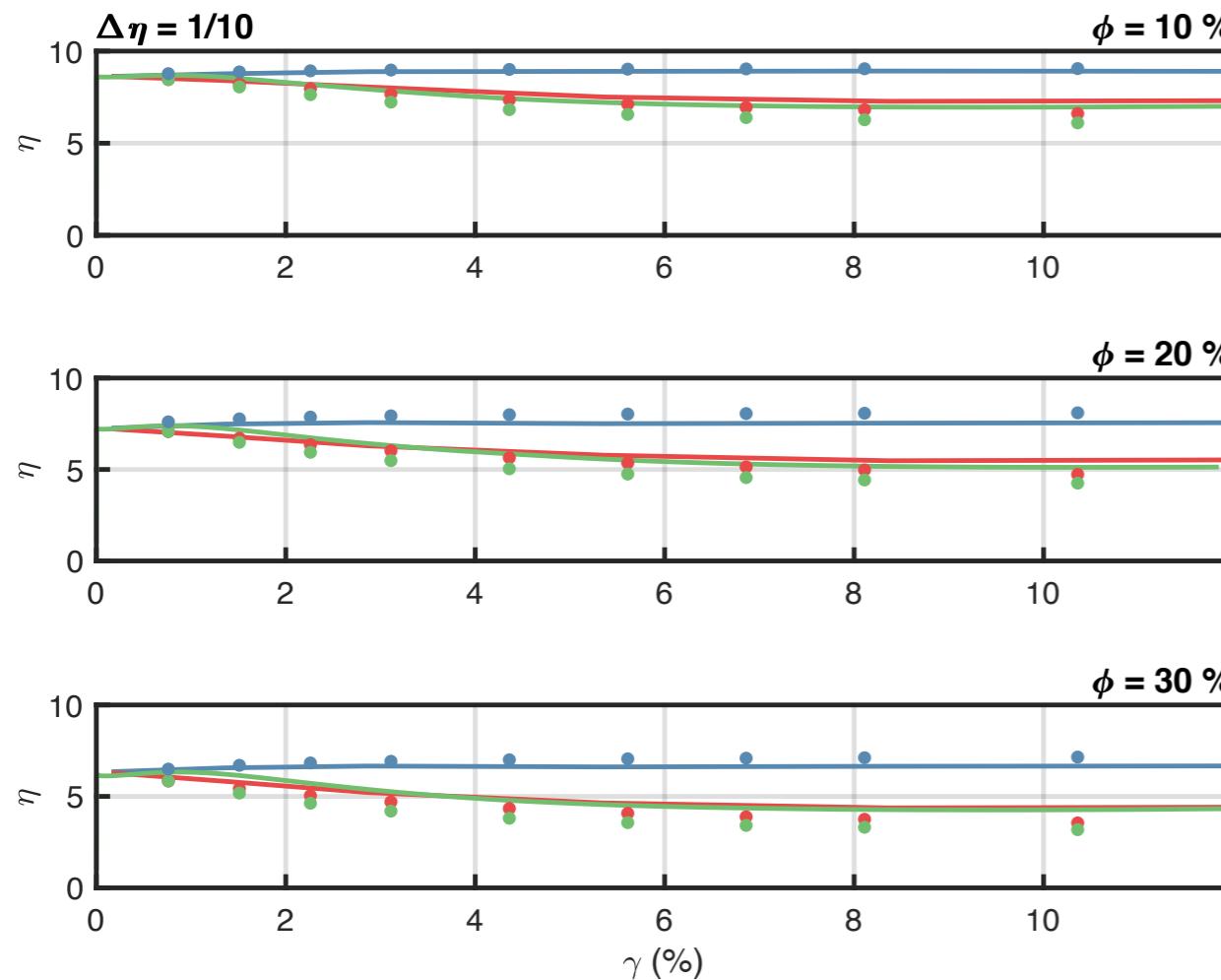


inclination = angle with respect to horizontal plane

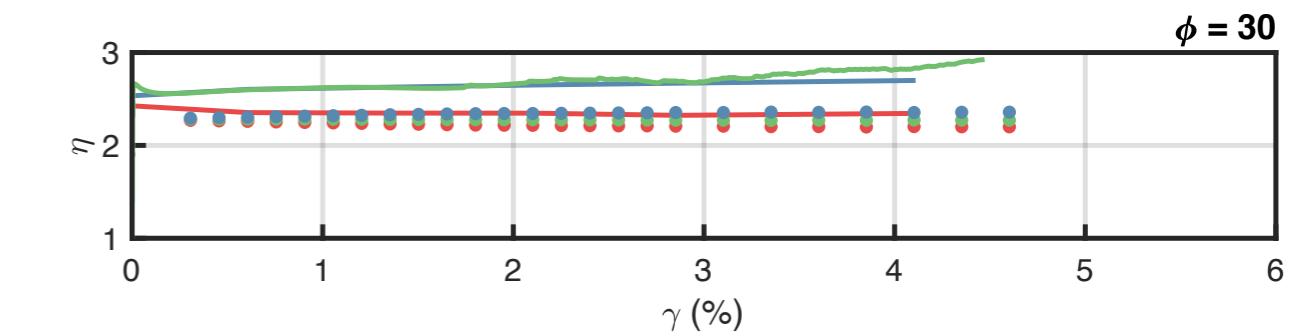
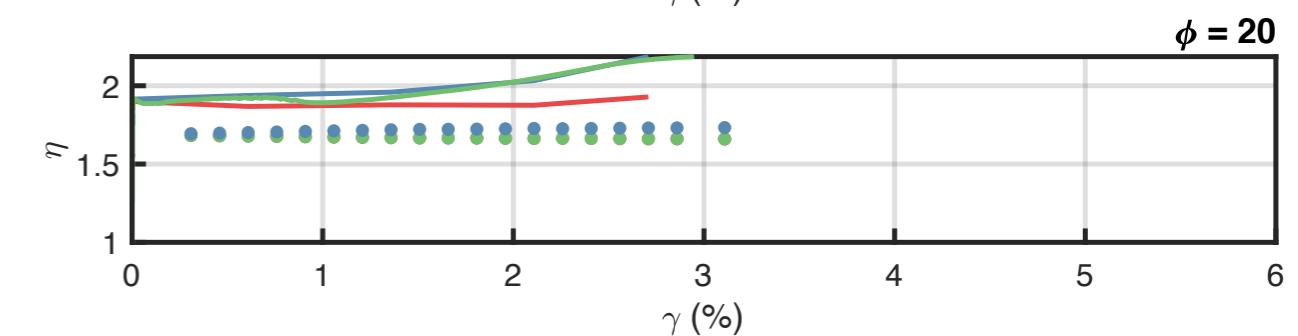
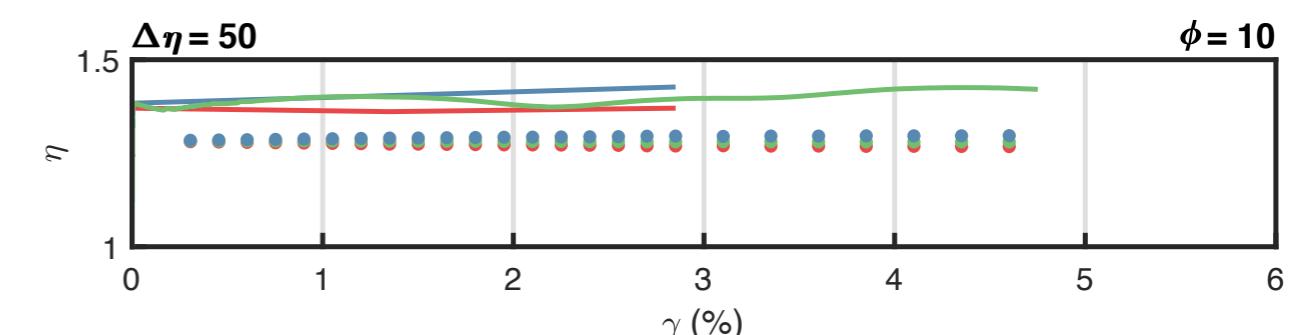
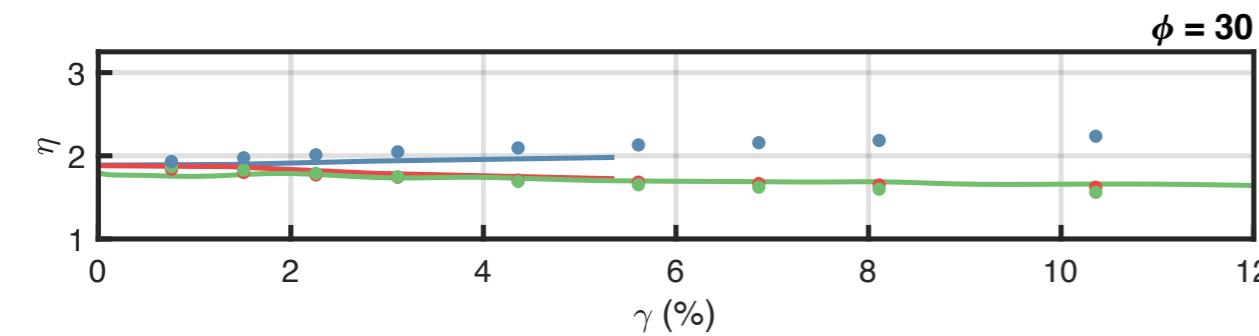
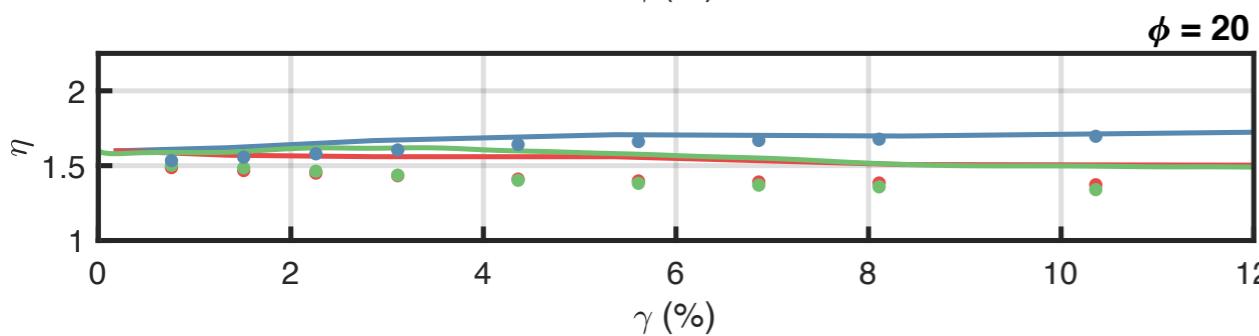
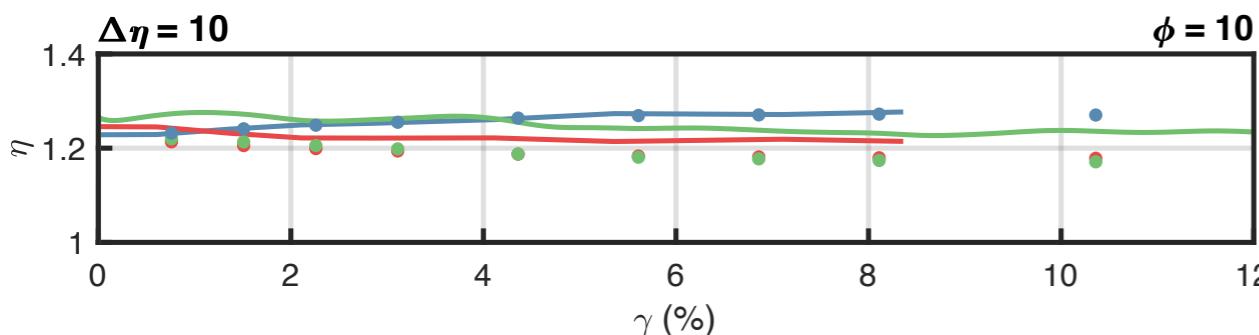
$a_i = i^{\text{th}}$  principal axis

$\phi = \text{volume fraction}$

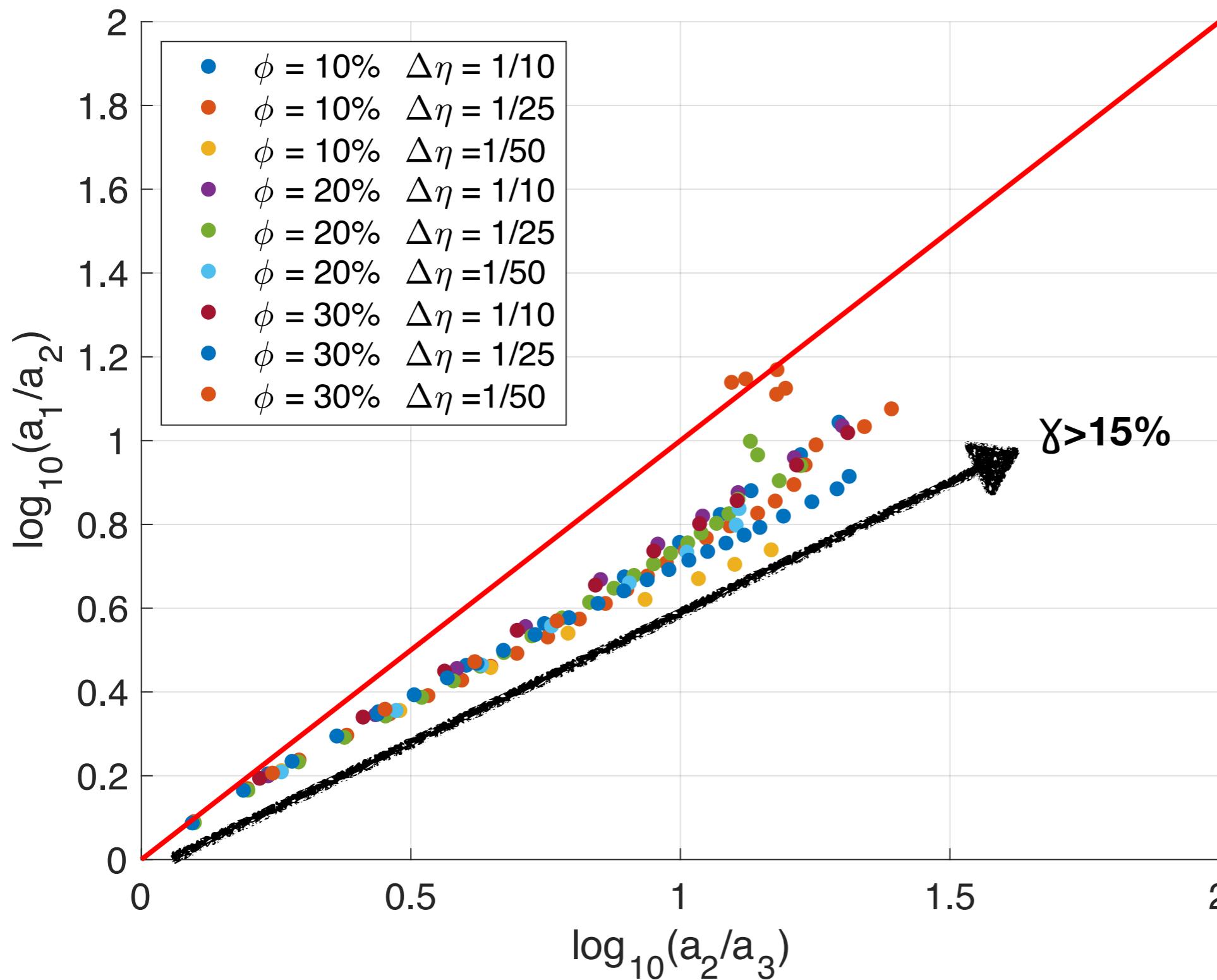
$\gamma = \text{shear strain}$



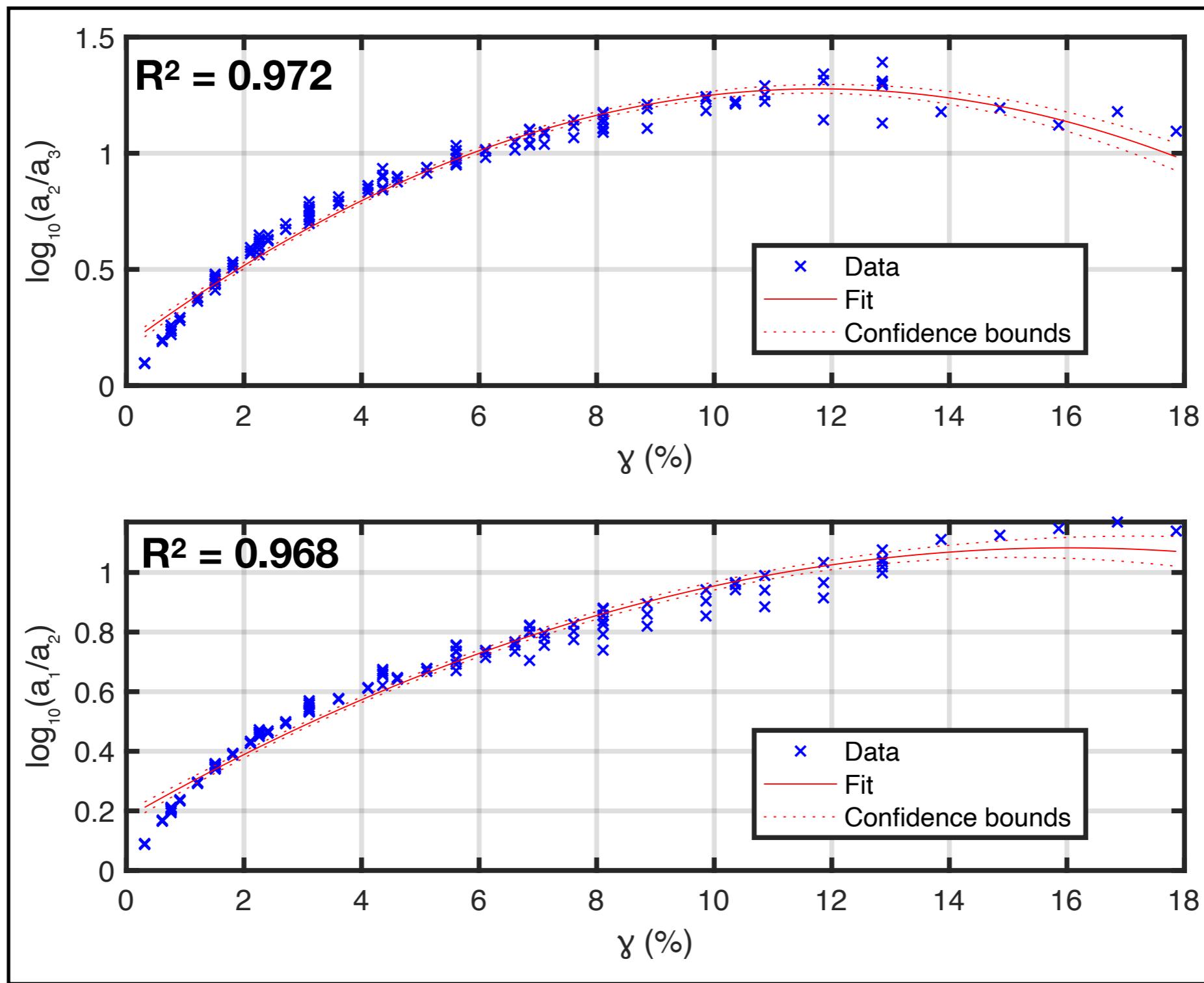
$\eta_{xz}$ $\eta_{xz}^{\text{DEM}}$	$\eta_{yz}$ $\eta_{yz}^{\text{DEM}}$	$\eta_{xy}$ $\eta_{xy}^{\text{DEM}}$
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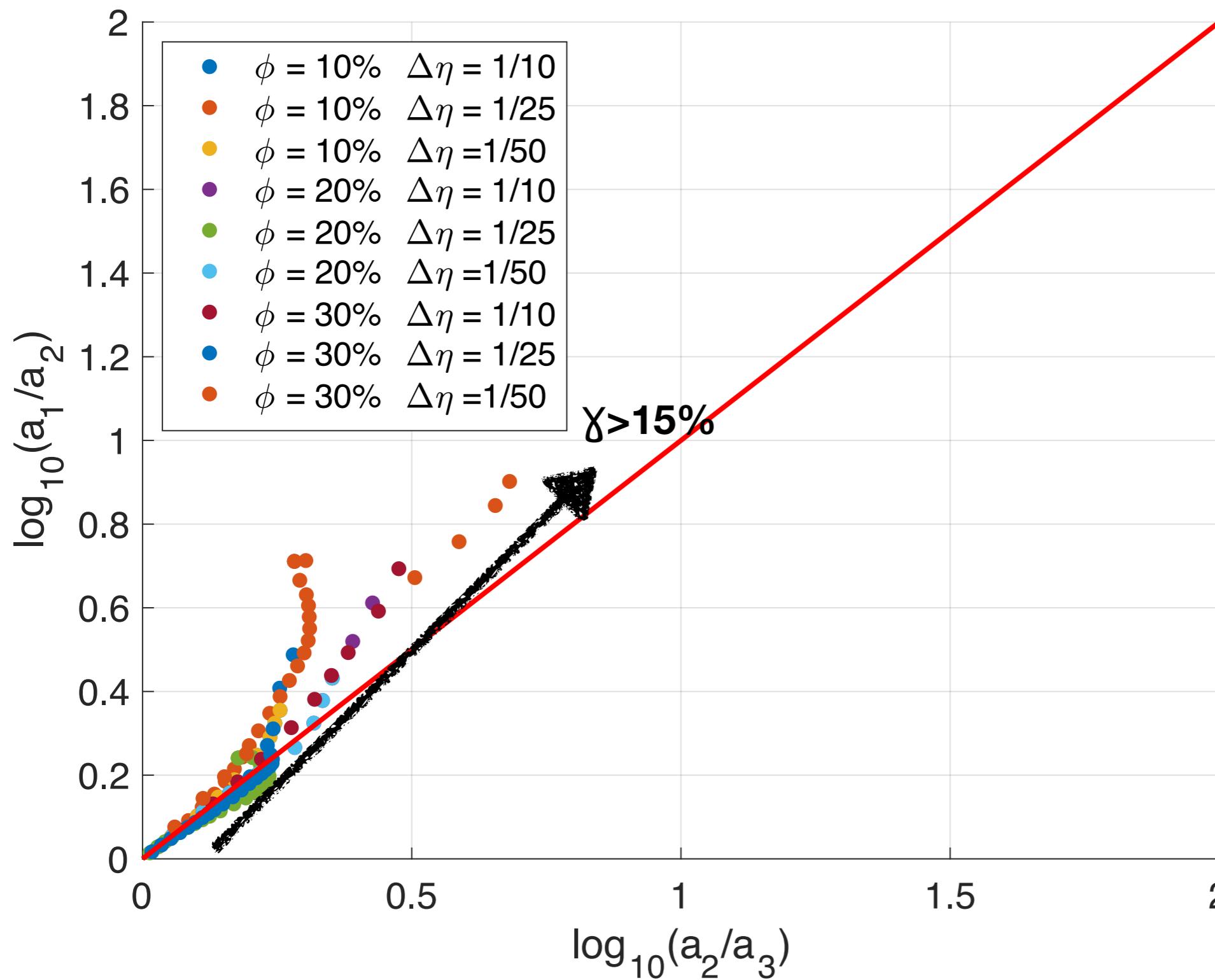
<span style="color: green;">—</span> $\eta_{xz}$ <span style="color: green;">•</span> $\eta_{xz}^{\text{DEM}}$	<span style="color: blue;">—</span> $\eta_{yz}$ <span style="color: blue;">•</span> $\eta_{yz}^{\text{DEM}}$	<span style="color: red;">—</span> $\eta_{xy}$ <span style="color: red;">•</span> $\eta_{xy}^{\text{DEM}}$
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$$\log_{10} \text{shape} \approx a + b \log_{10}(a_1/a_2)_{FSE} + c \log_{10}(a_2/a_3)_{FSE}$$



Inclusion average shape parametrised as function of the bulk Finite Strain Ellipsoid (FSE) and  $\sim$  independent of  $\phi$  and  $\Delta\eta$

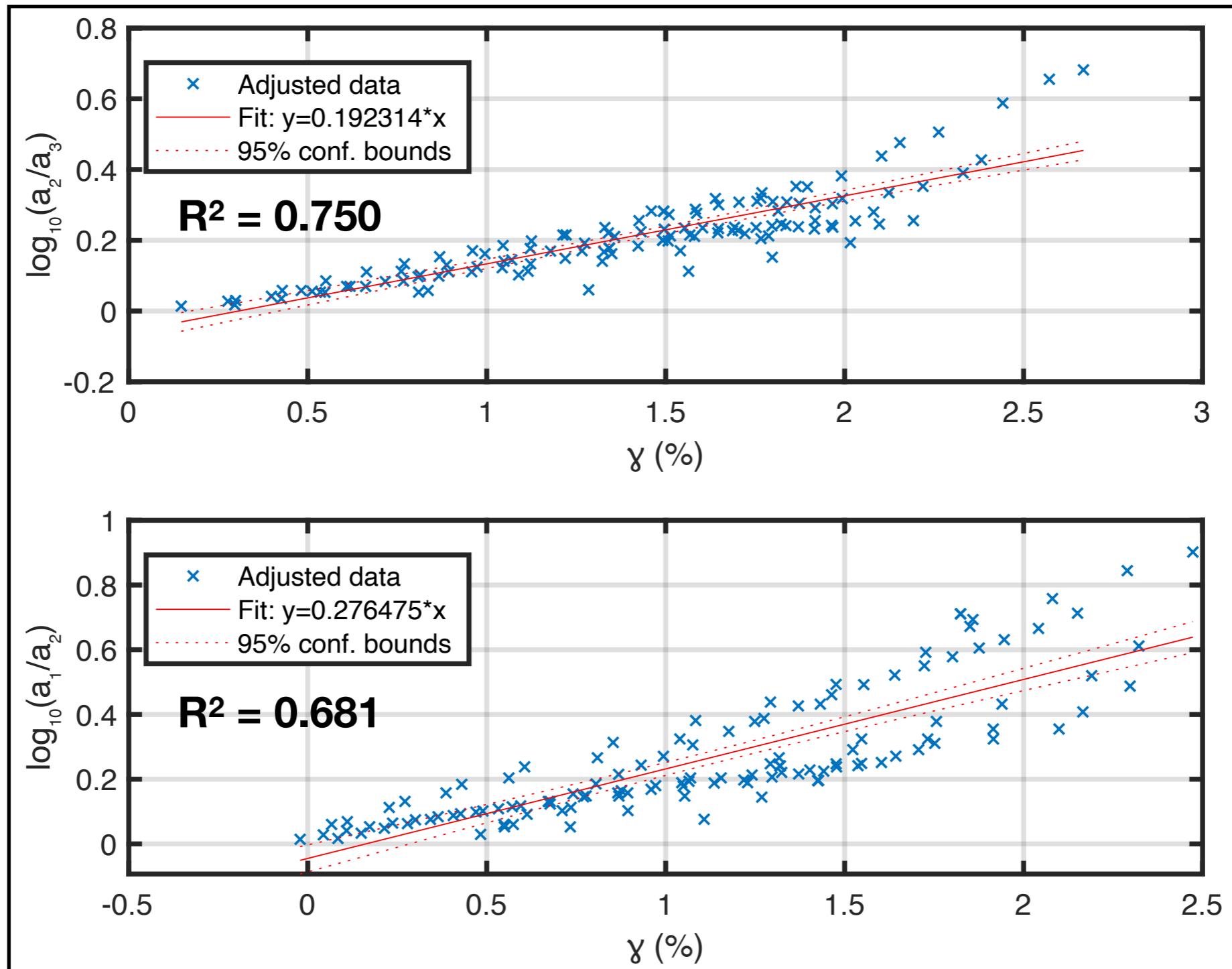
**FLINN DIAGRAM:**

Every circle represents the average shape of the inclusion phase at a given shear strain

# FABRIC PARAMETRISATION

Strong inclusions

$$\log_{10} \mathbf{shape} \approx a + b \log_{10}(a_1/a_2)_{FSE} + c \log_{10}(a_1/a_2)_{FSE}^2 + d \log_{10}(a_2/a_3)_{FSE} + e \log_{10}(a_2/a_3)_{FSE}^2 + f\phi + g\Delta\eta + h\Delta\eta^2$$

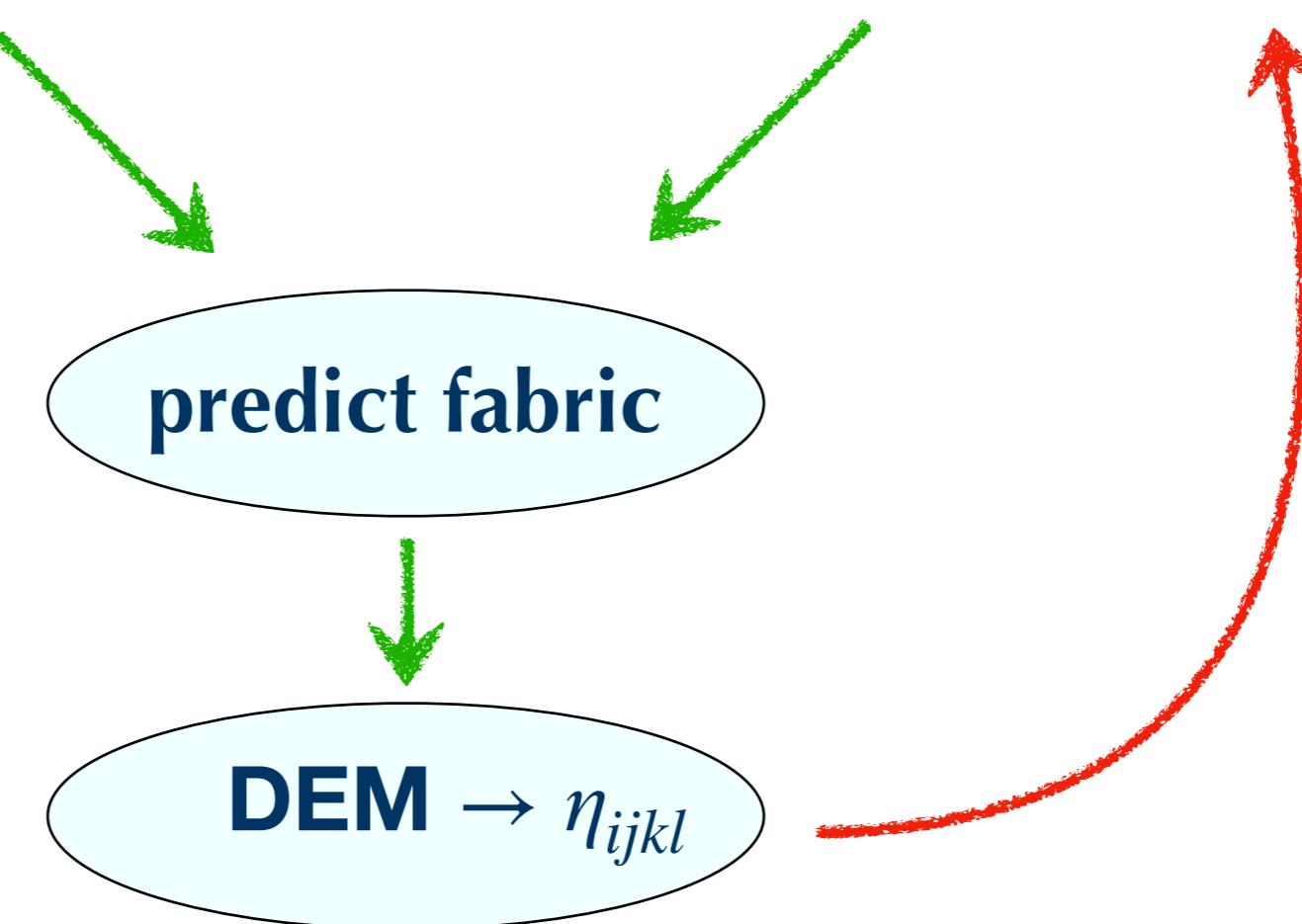


Inclusion average shape parametrised as function of the bulk Finite Strain Ellipsoid (FSE), volume fraction  $\phi$  and viscosity contrast  $\Delta n$

- Weak inclusions → planar fabric → strain localisation
- Strong inclusions → cigar-shaped
- The fabric can be parameterised as a function of shear strain, volume fraction and viscosity contrast
- Anisotropic viscous tensor of Newtonian-isotropic two-phase composites can be computed averaging the inclusion shape and using the DEM (max. errors ~10-15%)

**$t = 0$  : solve Stokes -> velocity, strain,...  
(isotropic material)**

**$t > 0$  : solve Stokes -> velocity, strain,...  
(anisotropic material)**



**Finite Strain Ellipsoid**

**Rotation matrix**

$$R = [v_1^T, v_2^T, v_3^T]$$



**Orientation**

**Particle shape**

$$\{a_1, a_2, a_3\}$$



**Fabric**

$a_i$  =  $i$ th eigenvalue of the FSE

$v_i$  =  $i$ th eigenvector of the FSE

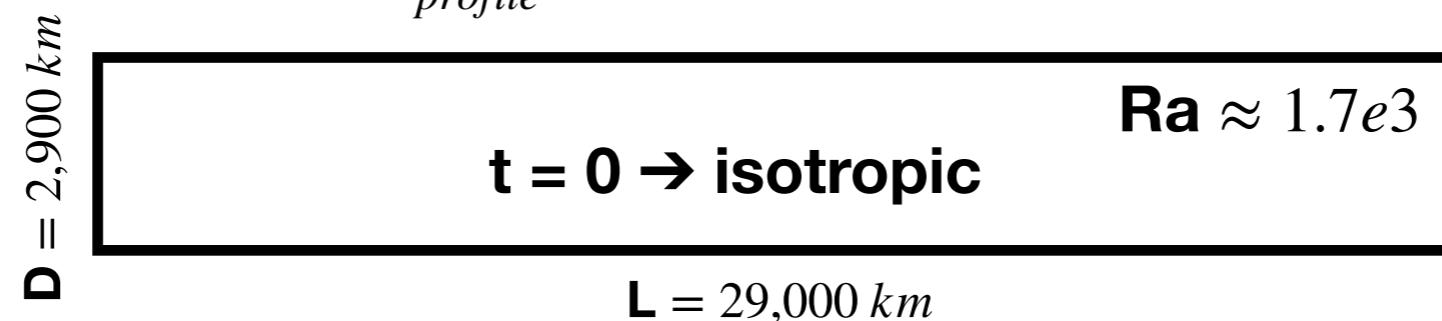
**Stokes equations:**

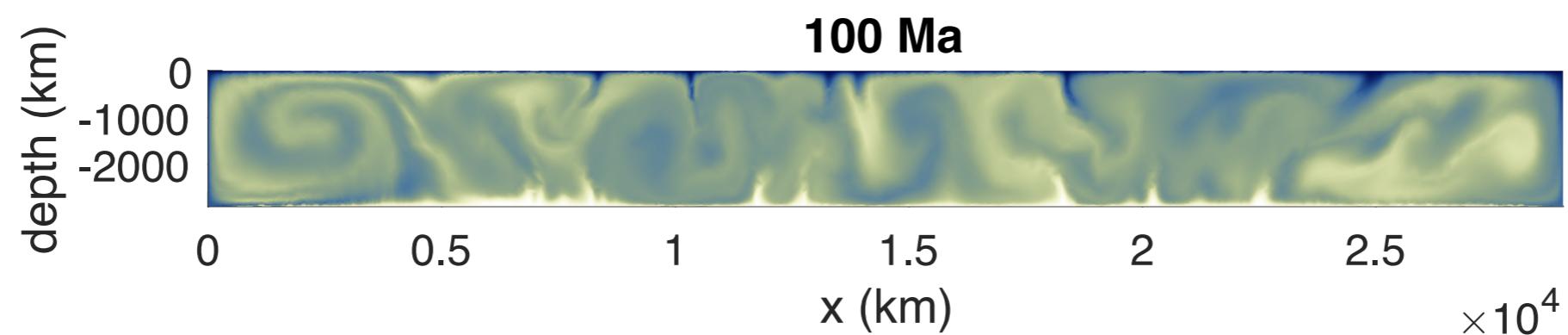
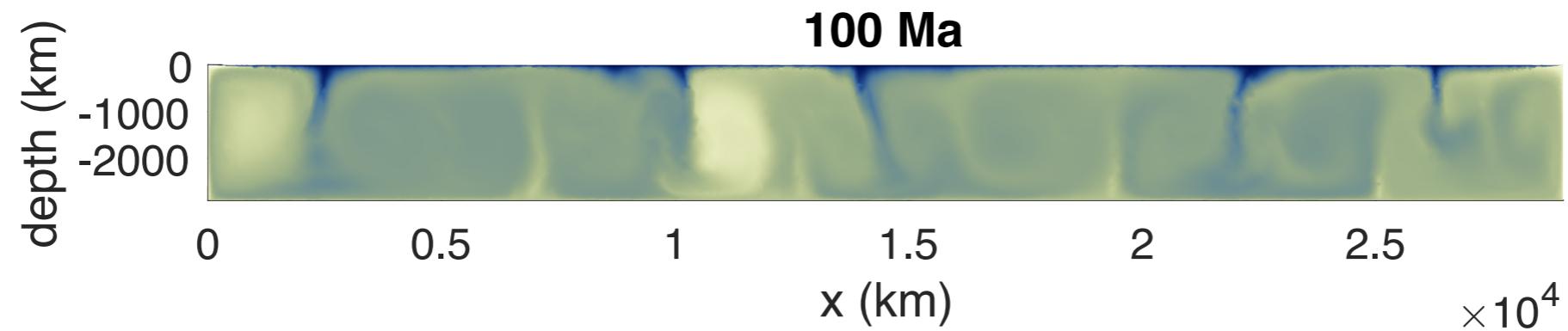
- Incompressible
- Lagrangian Finite Element Method
- Newtonian Rheology
- $\rho = \rho_o(1 - \alpha\Delta T)$

**Methods:**

1. Isotropic
2. Anisotropic (fabric defined @ t=0; does not evolve with time)
3. Anisotropic (isotropic @ t=0; fabric evolves following parametrisation))

$$T_{profile} = \text{adiabat} + \text{noise}$$



**(1) Isotropic****(2) Anisotropic (constant fabric)****(3) Anisotropic (evolving fabric)**