



## Advanced Bridge Monitoring Strategies by Polarimetric GB-SAR

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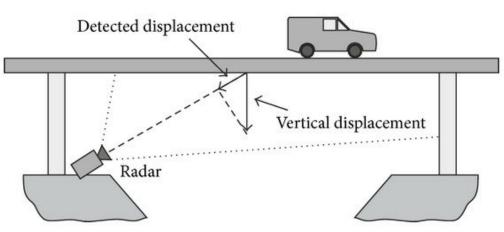


## Motivation and Objective

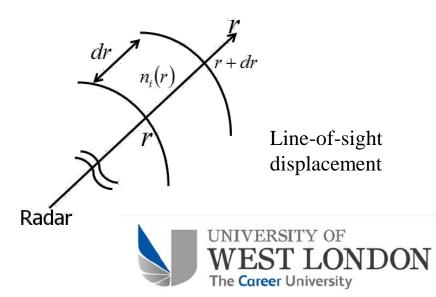


Bridge collapses (Italy, 2018)





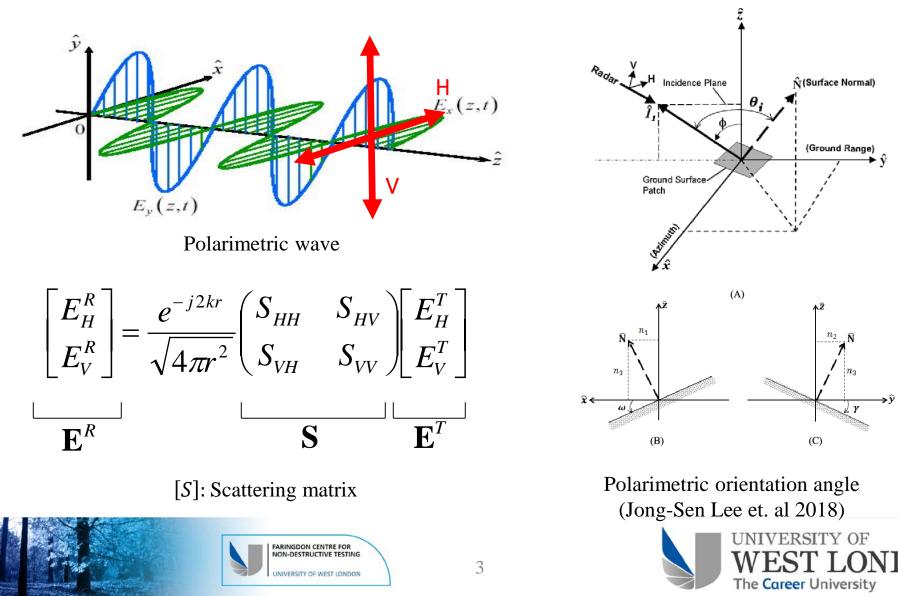
Bridge monitoring by Interferometry Radar (M. Pieraccini, 2013)



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#### Radar polarimetric and polarimetric orientation angle



# FASTGBSAR System



#### Polarimetric GB-SAR system





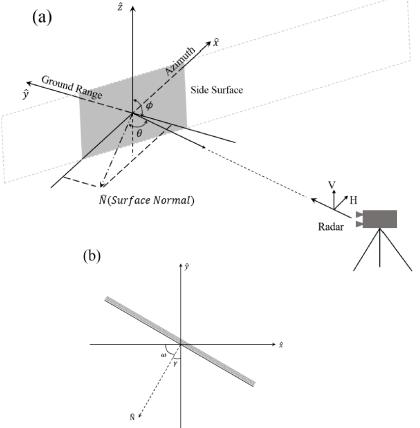
Parameter	Value
Operating frequency	17.2 GHz (Ku Band)
Range resolution	Up to 0.5 m
Maximum range	4 km
EIRP power	19 to 42 dBm
Operating temperature range	-25 °C to 60 °C
Sensor weight	10 kg
Accuracy	± 0.01 mm
Power consumption	70 W





### Field Measurement





Bridge monitoring by polarimetric GB-SAR system (Sendai, Japan)



(a) Radar imaging geometry of the side surface. (b) The side surface projection in both azimuth and ground range direction.



## Vertical Deformation Calculation

The polarimetric orientation angle (POA) can be expressed as:

$$\tan(-4\eta) = \frac{-4Re(\langle (S_{HH} - S_{VV})S_{HV}^* \rangle)}{-\langle |S_{HH} - S_{VV}|^2 \rangle + 4\langle |S_{HV}|^2 \rangle}$$
$$\xi = \begin{cases} \eta, & \text{if } n \le \frac{\pi}{4} \\ -\eta - \frac{\pi}{2}, & \text{if } n > \frac{\pi}{4} \end{cases}$$

where  $\xi$  indicates the POA. The POA can also be obtained from the azimuth slope angle  $\omega$ , ground range slope angle  $\gamma$ , and radar look angle  $\phi$  based on the imaging geometry by the following equation

$$\tan(\xi) = \frac{\tan\omega}{-\tan\gamma\cos\phi + \sin\phi}, -\frac{\pi}{2} \le \xi \le \frac{\pi}{2}.$$

The local incidence angle  $\theta$  can also be derived in terms of the local slopes and radar look angle, it can be expressed as:

$$\cos\theta = \frac{\tan\gamma\sin\phi + \cos\phi}{\sqrt{1 + \tan^2\gamma + \tan^2\omega}}$$

So that the radar look angle  $\theta$  can be calculated with the above equations, and the vertical deformation can be known.

