

## Introduction

The transport of reactive solute like Cr(VI) in groundwater environment can be largely influenced by adsorption/desorption process. In this process, the influence of the porous media with different properties, which causes heterogeneity to some extent, cannot be ignored. In this study, six different kinds of sediments were collected to investigate the adsorption and mobility of Cr(VI) in varied sediments using batch and column experiments. The results of batch experiments were described by three kinetic models and two equilibrium isotherms. Four model identification criteria were used to rank these alternative models and identify the sorption mechanism. The adsorption parameters derived from column experiments were compared with batch experiments. The results from this study provide important insight for us to understand the transport behaviors of Cr(VI) in porous media.

## China **S0**01 S003 - 47°15' II, $\Pi_1$ $I_1$ Low floodplain $I_2$ High floodplain $II_1$ Low hillock Plain

### Materials and methods

A study site under threats, which is a typical alluvial valley plain in the north east of China, was chosen for the sample collection. The study site has been in a fluvial and lacustrine sedimentary environment and deposited thick Pleistocene unconsolidated sediments since the Quaternary.

II<sub>2</sub>Low undulating plain Rivers and Lakes Figure 1. Geological localization of sediments used in this work.

We collected the six sediment samples along the transverse direction. 
Table 1
Table 2

Partic	cle size	and sed	iment ty	/pe cl	naracterization	n Mai	n che	mical a	nd mine	eral co	ompoi	nents	(%)
	Clay (%)	Silt (%)	Sand (%)	SSA	type	Samp	Quart	Plagiocl	C l a y	$Al_2O_3$	Fe <sub>2</sub> O <sub>3</sub>	FeO	LOI
						les	Ζ	ase	minerals				
	< 0.002	0.002-	0.02-0.2			S001	33	20	24	13.94	3.08	0.54	2.01
	mm	0.02 mm	mm			\$002	40	8	43	14 22	3 17	0.52	2 84
S001	2.69	6.33	90.98	0.086	Loamy sand	5002	τU	0	J	17.22	J.17	0.52	2.04
S002	5.83	22.12	72.05	0.185	Sandy loam	S003	32	14	36	13.94	2.88	0.59	2.1
S003	2.08	6.06	91.86	0.066	Loamy sand	S004	34	17	42	16.09	3.21	0.63	5.99
S004	16.35	58.75	24.90	0.481	Silty loam clay	GOOF	07	11		146	2.45	0.60	4.00
S005	10.41	44.30	45.29	0.332	Loam	S005	27		57	14.6	3.45	0.63	4.28
S006	7.74	29.81	62.45	0.246	Sandy loam	S006	35	13	41	13.96	3.06	0.52	3.42

All the batch experiments were performed at room temperature ( $25 \pm 1$ ) °C) in the SHA-C oscillator at a rate of 200 rpm. Each sample in a conical flask contains 2 g soil and 50ml solution. In kinetic experiments, the concentration of Cr(VI) was 5 mg/L in initial solution. Then the Cr(VI) was analyzed at different time intervals. In

# Sorption model identification for chromium transport in unconsolidated sediments

Yang Cao<sup>1</sup>, Zhenxue Dai<sup>1</sup>, Xiaoying Zhang<sup>1</sup>, and Ziqi Ma<sup>1</sup> <sup>1</sup>College of Construction Engineering, Jilin University, Changchun, China

equilibrium experiments, concentrations of Cr(VI) in graded levels were contained in the samples, i.e., 2, 5, 10, 20, 30, 40 and 50 mg/L. The transport experiments were carried out in the plexiglass columns. The diameter of the column used for the S001, S002 and S003 was 6cm and the filling height was 10cm. Smaller column with 2cm diameter was used for S004, S005 and S006 and filling height was 1 cm.

### Kinetic and equilibrium models

### Kinetic models

pseudo-first-order model:  $\ln \left(1 - \frac{q_t}{q_e}\right) = A + k_1 t$  Henry model:  $q_e = K_H C_e$ pseudo-second-order model:  $\frac{t}{q_t} = \frac{1}{k_2 q_e^2} + \frac{t}{q_e}$ Elovich model:  $\frac{q_t}{q_e} = R_e \ln\left(\frac{t}{t_e}\right) + 1$ 

### Model selection criteria

Promoted by the development of maximum likelihood theory, model selection criteria for evaluating model simplifications and processconceptual models have been established successively, such as (Dai et al.,2012; Ye et al., 2008). The Akaile Information Criterion (AIC) proposed by Akaile is the most popular criterion (Akaike, 1974),  $AIC_k = N_Z \ln \widehat{\sigma}_{ML}^2 + 2P_k$ 

where  $N_z$  is the number of data;  $P_k$  is the number of estimated parameters; k indicates the kth alternative process-conceptual model, k = $\overline{1, K}$ . N<sub>z</sub> ln  $\widehat{\sigma}_{ML}^2$  is a term obtained from unbiased least square estimator,

 $\widehat{\sigma}_{ML}^2 = \frac{\Psi}{N_{T}}$ 

where  $\phi$  is the generalized sum of squares residuals. In AIC, a deviation affecting the accuracy occurs when  $N_Z / P_k < 40$ . In order to correct this deviation, (Hurvich and Tsai, 1989) considered the calibration data set size and proposed a more reliable modified Akaile information criterion (AICc),

$$AIC_{C_k} = N_Z \ln \widehat{\sigma}_{ML}^2 + 2P_k^2$$

Based on the background of Bayesian information, (Schwarz, 1978) deduced the Bayesian information criterion (BIC),

 $BIC_k = N_z \ln \hat{\sigma}_{ML}^2 + P_k \ln N_z$ 

Another consistent criteria, Hannan information criterion (HIC), have been introduced by (Hannan and Quinn, 1979). HIC=N<sub>Z</sub> ln  $\hat{\sigma}_{ML}^2$  + 2N<sub>Z</sub> ln(ln P<sub>k</sub>)

Our data analysis applies least squares approach. Therefore,  $\phi$  can be obtained and values of AIC, AICc, BIC, and HIC are calculated in this study. The best model has the lowest values of AIC, AICc, BIC, and HIC.

### Equilibrium models

Langmuir model:  $q_e = \frac{q_m K_L C_e}{1 + K_L C_e}$ Freundlich model:  $q_e = K_F C_e^{\frac{1}{n}}$ 

 $\frac{2P_k(P_k+1)}{N_z - P_k - 1}.$ 

According to the model selection criteria, the results are not exactly the same with correlation coefficients. As for sorption kinetics, it is found that Elovich equation is superior to the other two models to describe the kinetic data of S006. And S001, S004 has the best fitness to pseudo first order equation. As for sorption equilibrium, Langmuir model is more favorable than Freundlich model for S001, S002 and S003. Model selection criteria are more sensitive to the performances of different model fittings and can make the differences more intuitive.

Elovich Pseudo Pseudo

HIC 31.08 15.12 According to the parameters obtained from model fitting, in both batch and column studies, particle size distribution and the clay mineral contents were the most important factors affecting adsorption capacity and adsorption rate.

Dai, Z. et al., 2012. Identification of sorption processes and parameters for radionuclide transport in fractured rock. Journal of Hydrology, 414: 220-230. Ye, M., Meyer, P.D., Neuman, S.P., Pacific Northwest National Lab, R.W.A., 2008. On model selection criteria in multimodel analysis. Water Resources Research, 44(3): W03428

Akaike, H., 1974. A new look at the statistical model identification, Selected Papers of Hirotugu Akaike. Springer, pp. 215-222. Hurvich, C.M., Tsai, C.-L., 1989. Regression and Time Series Model Selection in Small Samples. Biometrika, 76(2): 297-307. Hannan, E.J., Quinn, B.G., 1979. The determination of the order of an autoregression. Journal of the Royal Statistical Society: Series B, 41(2): 190-



## Results

				Table 4 Model	4 parameter	s calcula	ted from L	angmuir	and Fro	eundlich a	dsorption	models		
Pseudo	second o	rder			Henry's			h		Langmu	Langmuir			
k <sub>2</sub>	$q_e$	$\mathbb{R}^2$	Expect		K <sub>H</sub>	R <sup>2</sup>	K <sub>F</sub>	n	R <sup>2</sup>	KL	q <sub>m</sub>	R <sup>2</sup>		
0.0342	5.23	0.006/	$\frac{\text{ed } q_e}{5}$	S001	0.8974	0.9954	1.5987	1.1921	0.9982	0.0080	145.4441	0.9992		
0.0342	12.02	0.0007	J 11 7	S002	1 0040	0.0702	6 9369	1 5737	0 9908	0.0301	131 2814	0 9980		
0.0222	12.02	0.998/	11./	5002	1.9049	0.9703	4.5454	1.5757	0.0001	0.0301	56 4204	0.0000		
0.0299	9.07	0.9989	8.9	8003	0.9787	0.9565	4.5454	1./666	0.9881	0.0445	56.4204	0.9980		
0.0001	44.50	0.9853	43	S004	3.8232	0.9392	24.1317	2.1448	0.9790	0.0764	172.0555	0.9191		
0.0002	68.43	0.9937	69.15	S005	6.4300	0.8881	59.8972	2.9213	0.9918	0.1968	222.3172	0.9331		
0.0006	24.24	0.9975	21.45	S006	2.6827	0.9839	7.7114	1.4321	0.9948	0.0176	244.9329	0.9826		
ICc, B rption Henry's	IC, HI models s Freur	C from 1	L <b>angmui</b> Langmuir	rand 3	35 30 -	k <sub>d</sub> -	batch							
0.72	4 1 1		0.20		-	k <sub>d</sub> -	column							
0.75 9.53	-4.11 _1 11	_	9.29 6.29	2	5	u								
8.68	-4.21	_	9.40	2										
8.07	-5.44	-	10.63		ŀ									
31.96	16.15	5 5	5.44	2										
32.76	19.15	5 8	3.44	2										
31.91	16.04	4 5	5.33	py	ŀ									
31.29	14.82	2 4	1.10	1	5									
25.56	7.72	-	4.74	1	. <b>&gt;</b> F									
26.36	10.72	2 -	1.74						-					
25.51	7.61	-	4.84											
24.89	6.38	-	6.07	1	0									
45.81	28.52	2 3	37.94											
46.61	31.52	2 4	0.94		t						2			
45.76	28.41	1 3	87.83		5 L									
45.14	27.18	3 3	86.61		5									
56.62	27.53	3 4	2.17		-									
57.42	30.53	3 4	5.17											
56.56	27.42	2 4	2.06		0									
55.95	26.19	) 4	0.84		S00	1 50	02 50	03 5	004	S005	S006			
31.75	16.46	5 2	24.86		500	1 00	50	5 5		5005	5000			
32.55	19.46	5 2	27.86		Eiguro 2	Compo	ricon of t	ha diatri	ibution	coofficio	nt dorivos	from		
21.00	16.24		4 7 6		Figure Z	. Compa			DULION	COEIIICIE				

batch and column experiments

## Conclusions

the adsorption capacity increased as a function of particle specific surface area and the clay mineral contents

The mobility of Cr(VI) in different sediments has a sequence of: Loamy sand, sandy loam, silty loam clay, loam.

model selection criteria were superior to the error equations when comparing kinetic and equilibrium models because they took into account the quality of data and the complexity of the model.

## References