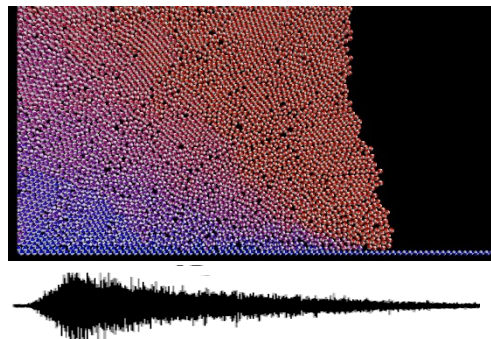


Simulations of the Basal Forces Generated by Dam Breaks: Comparison Between Continuous and Discrete Models

Hugo Martin^{1,2,3}, Bertrand Maury^{4,5}, Aline Lefebvre-Lepot⁶, Yvon Maday², Sylvain Viroulet⁷ &

Anne Mangeney^{1,2,3}



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²Sorbonne Université (LJLL)

³Inria Paris (Ange)

⁴Université Paris-Sud (LMO)

⁵École Normale Supérieure (DMA)

⁶École Polytechnique (CMAP)

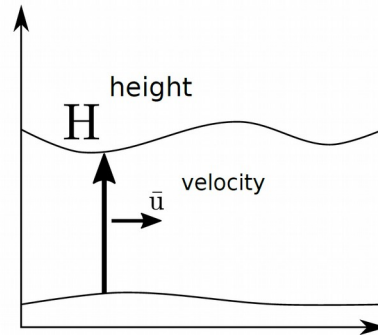
⁷Université Toulouse (IMFT)



Different Model Strategies

Quantitative comparison between the models and with laboratory experiments ?

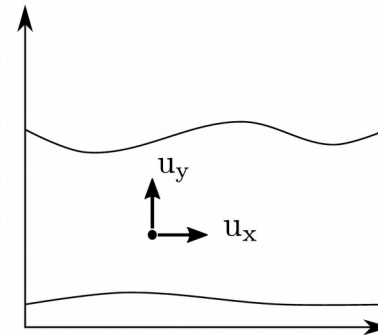
- Shallow-Water continuum equations



SHALTOP

*Bouchut et al. 2003,
Mangeney et al. 2007*

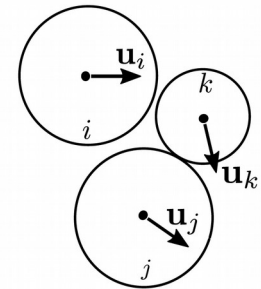
- Navier-Stokes continuum equations



BASILISK

Lagrée et al. 2011

- Discrete Elements Methods (DEM)



SCoPI

Maury et al. 2005

Decrease computational cost !



Landslide in Tuialamu. Photo/ Land Transport Authority Samoa

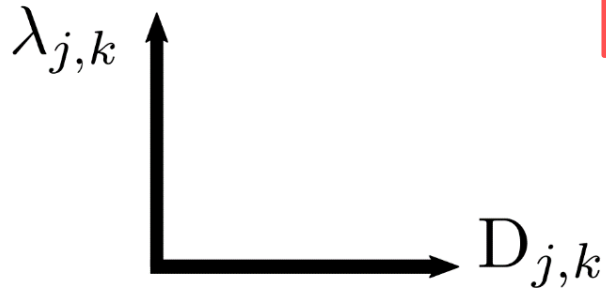


Discrete Elements Method: Contact Dynamics

For each particle:

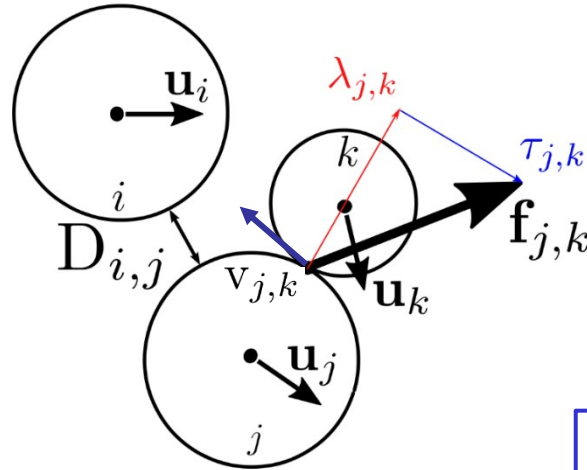
$$m_i \frac{d \mathbf{u}_i}{d t} = m_i \mathbf{g} + \sum_{j=i}^N \mathbf{f}_{i,j}$$

- Signorini's law

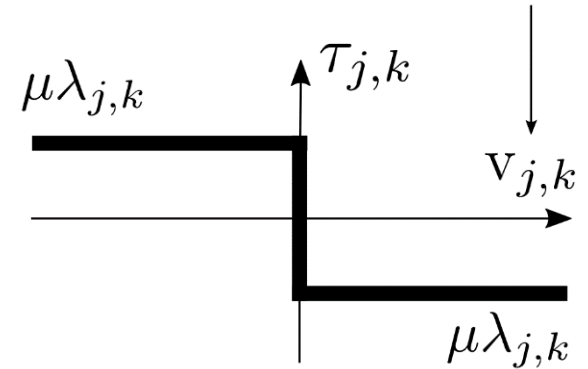


Equivalent to the *constraints* :

$$\begin{aligned} \lambda_{j,k} &\geq 0 \\ D_{j,k} &\geq 0 \\ \lambda_{j,k} D_{j,k} &= 0 \end{aligned}$$



- Coulomb's law Tangential relative velocity



Equivalent to
maximize the dissipated power :

$$\begin{aligned} \max_{\tau_{j,k}} \quad & -\tau_{j,k} v_{j,k} \\ \text{such that} \quad & |\tau_{j,k}| \leq \mu \lambda_{j,k} \end{aligned}$$

DEM with global computation of friction effects

Constrained optimisation problem *Stewart 2000, Moreau 2003*

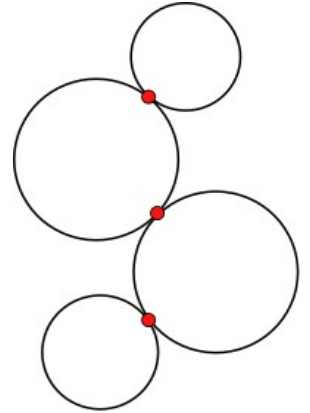
Term from frictionless model (normal forces)

$$\max_{\mathbf{u}, \boldsymbol{\lambda}, \boldsymbol{\tau}} \mathcal{F}(\mathbf{u}, \boldsymbol{\lambda}) - \boldsymbol{\tau} \cdot \mathbf{v}_t(\mathbf{u})$$

such that Newton's laws are verified and :

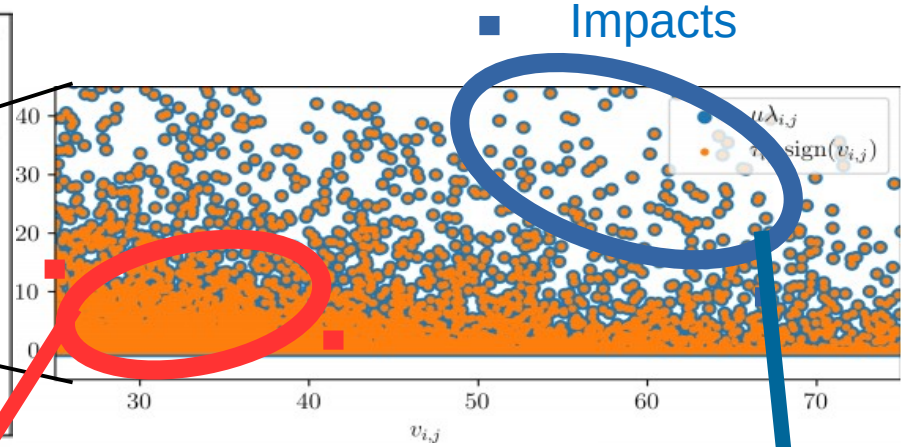
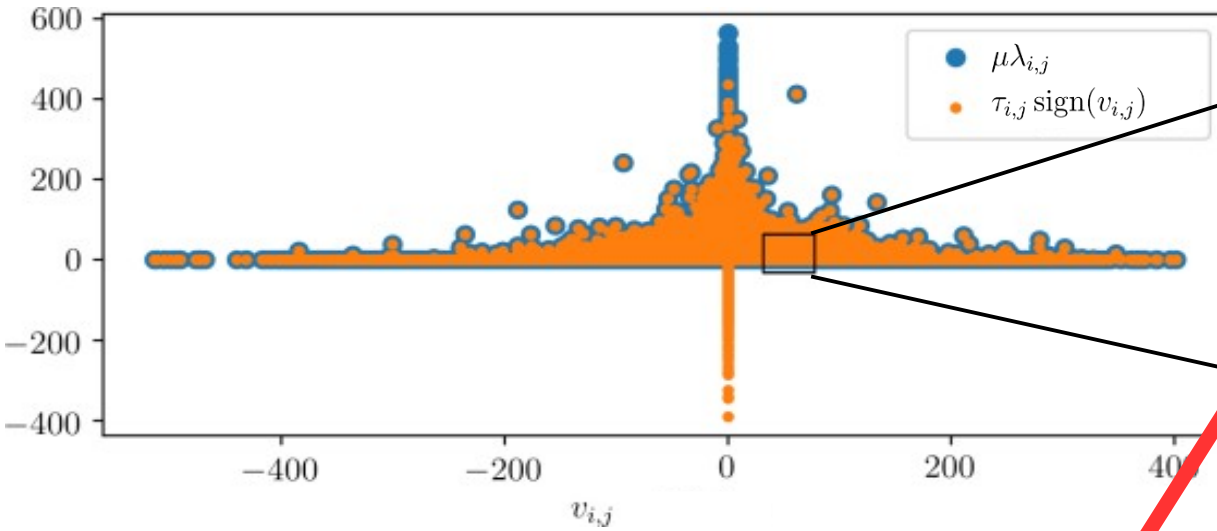
$$\begin{aligned} |\boldsymbol{\tau}| &\leq \mu \boldsymbol{\lambda} && \text{Coulomb's friction law} \\ \boldsymbol{\lambda} &\geq 0 && \text{Repulsive normal forces} \end{aligned}$$

Global dissipated power of tangential forces



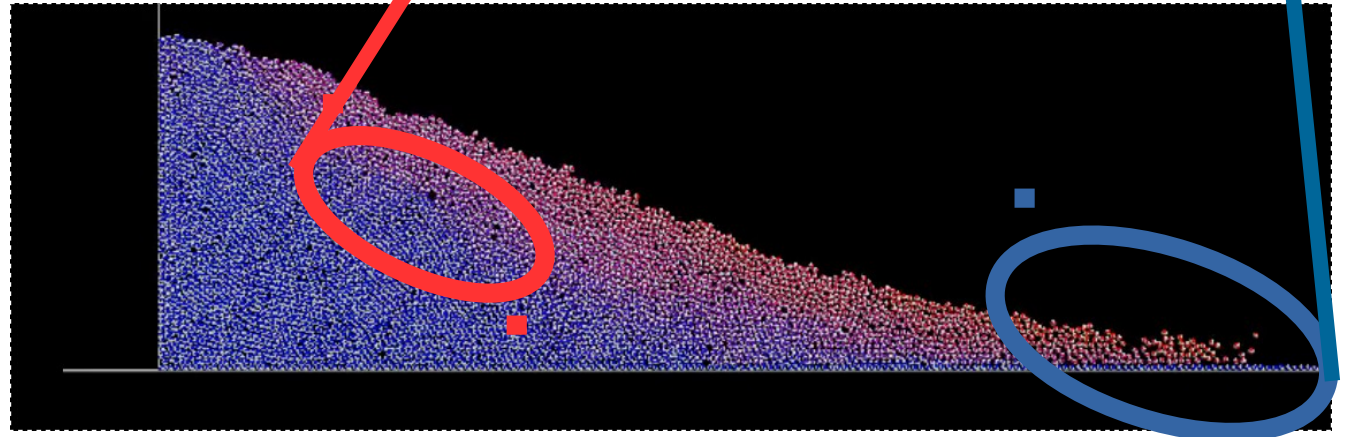
- Convex functional (numerically solved MOSEK)
- **Global computation of contact forces**
stable implicit-scheme
- **No iteration on the contact network !**

Local Coulomb's law



Coulomb's law :

$$v_{i,j} \neq 0 \quad \Rightarrow \quad |\tau_{i,j}| = \mu\lambda_{i,j}$$



2D Dam break over horizontal rigid bed

Continuum model rheology: $\mu(I) = \mu_s + \frac{\mu_2 - \mu_s}{I_0 + I} I$

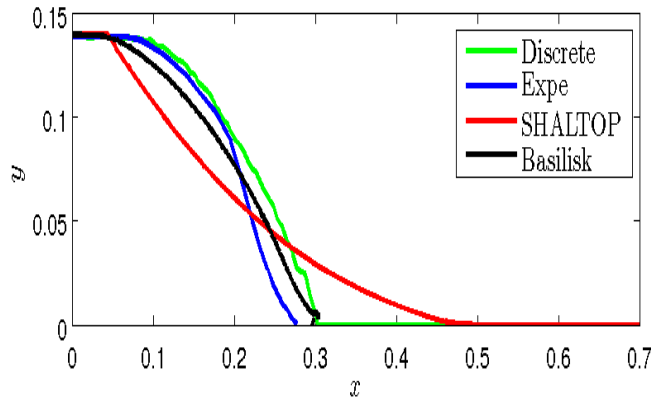
$$\mu_s = 0.48, \Delta\mu = 0.25 \quad \text{and} \quad I_0 = 0.279$$

Martin et al., 2017

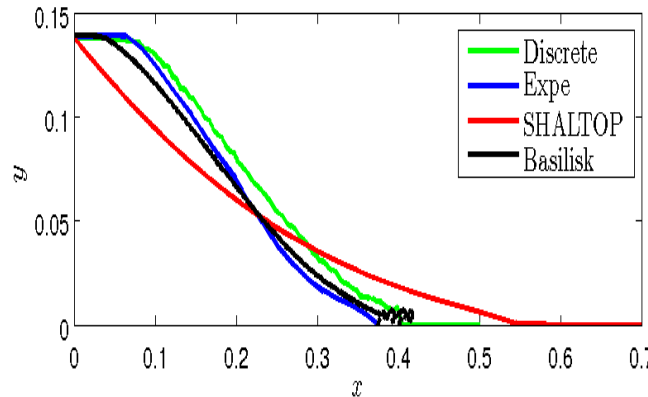
Discrete Element Method

Grain-grain friction coefficient: $\mu = 0.9$

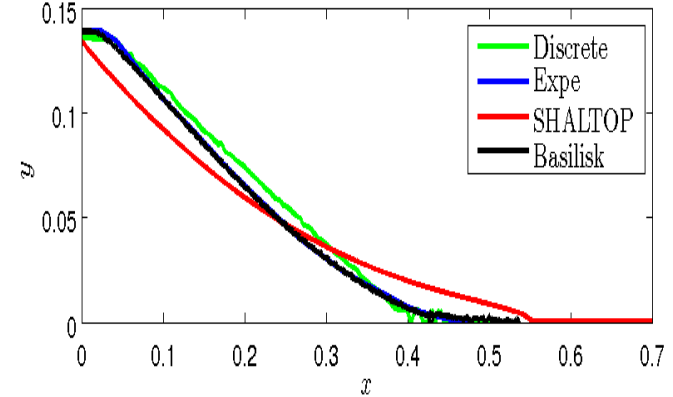
$t = 0.18 \text{ s}$



$t = 0.30 \text{ s}$



$t = 1.02 \text{ s}$



3D discrete method is in good agreements with experiments data when $\mu = 0.3$

Previous studies used additional dissipation (e. g. rolling friction) *Girolami et al. 2012*

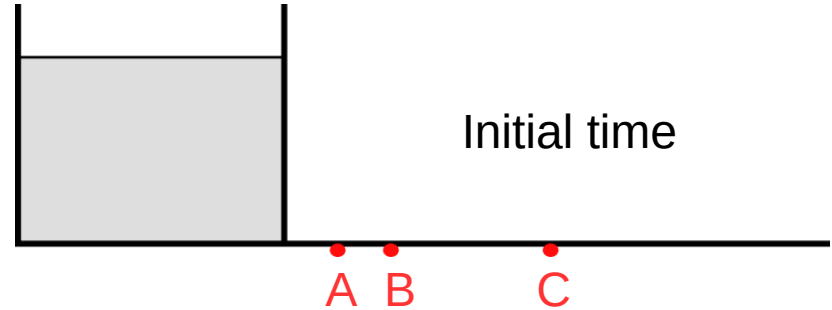
Viroulet et al., 2019

Basal forces

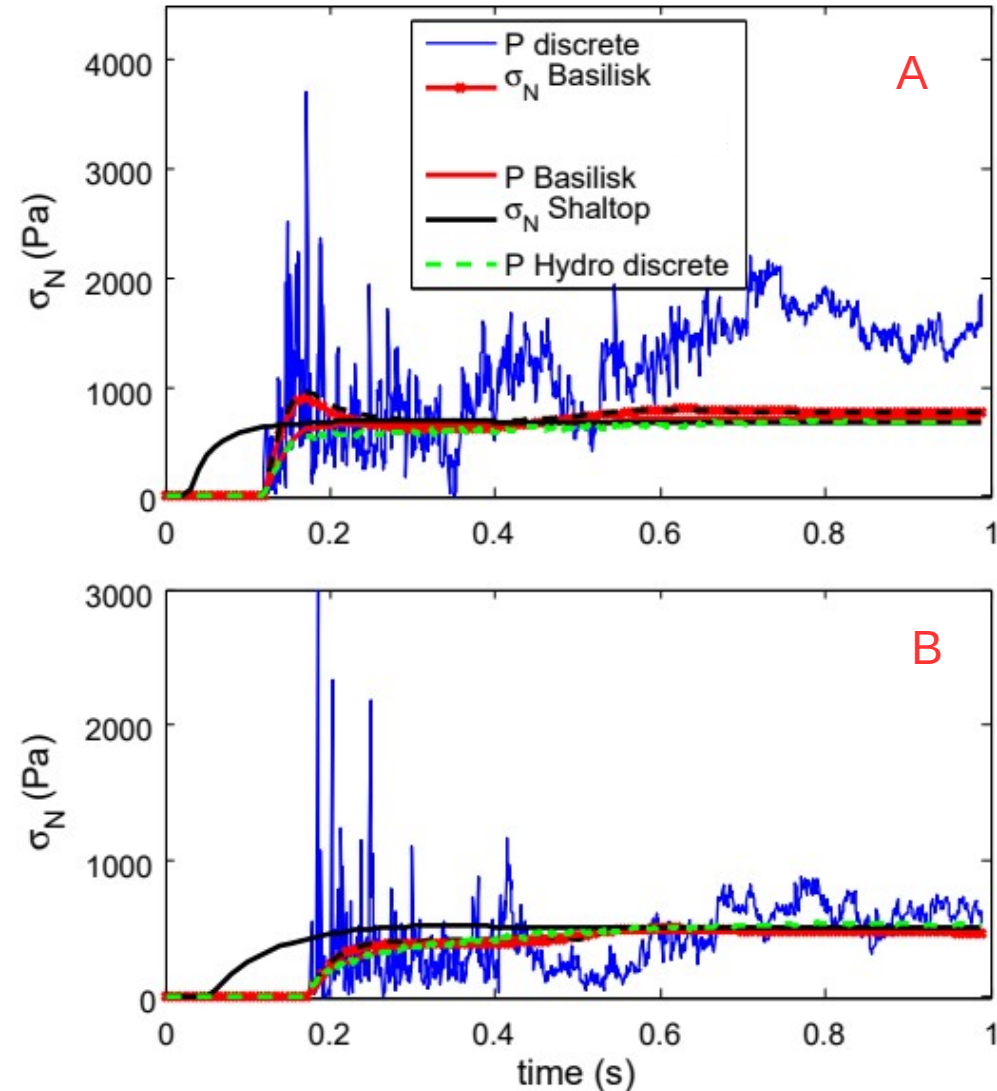
N = 65 909 discs

Computation time : 47h 31mn

2 Intel Xeon E5-2650 2.00 GHz (2x8 cores)

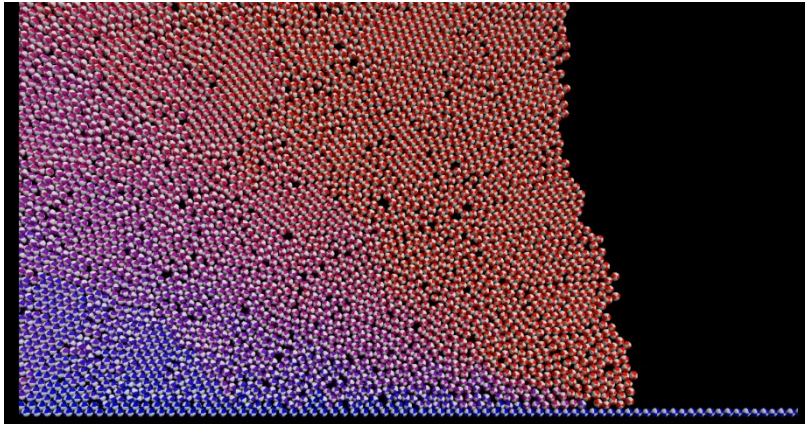


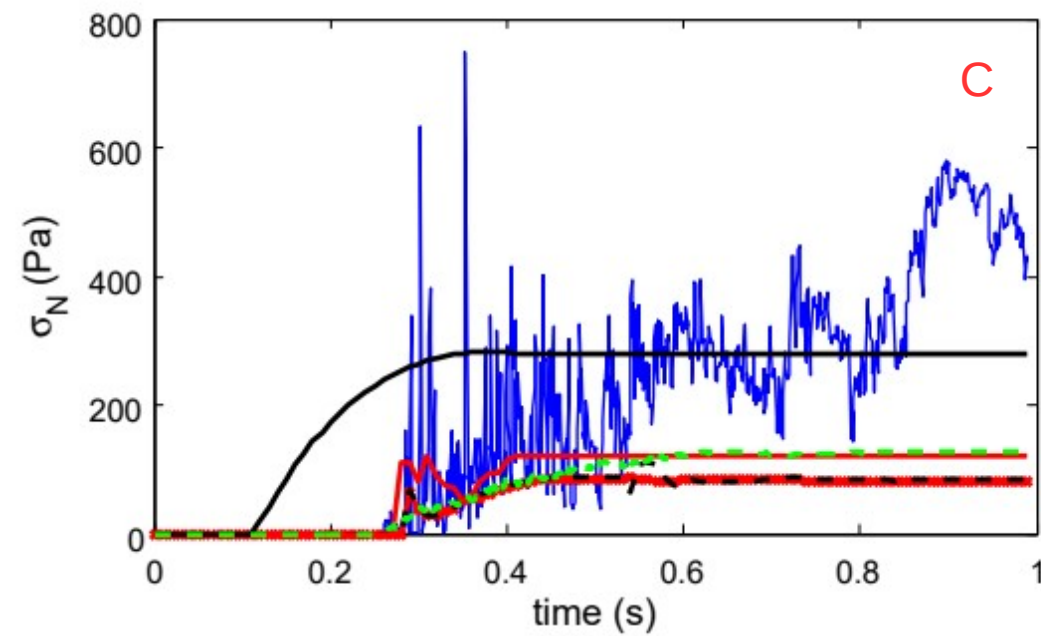
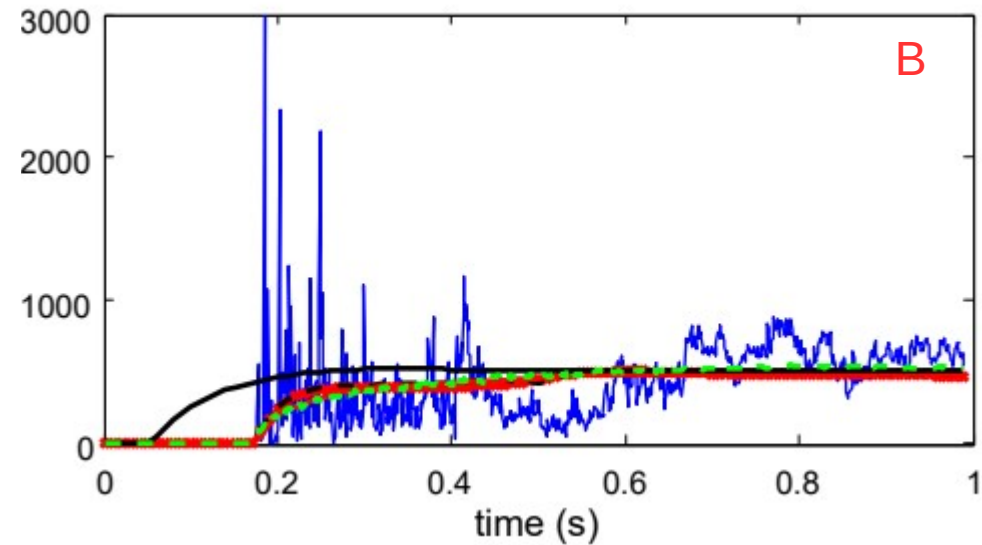
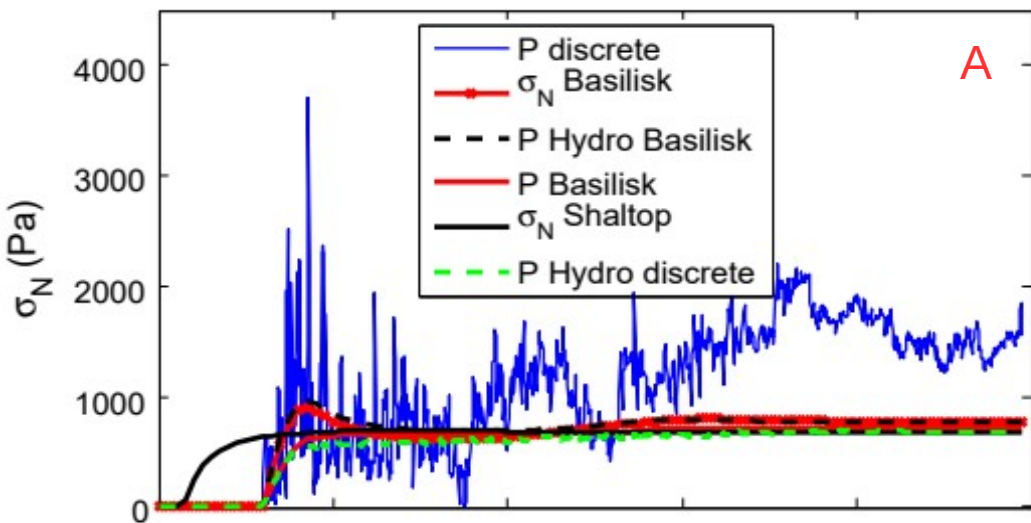
Strong fluctuations and spatial variability of the basal forces calculated from Discrete Element Methods !



Conclusion & Perspective

- **Global Model** for the Dry Friction Problem in Contact Dynamics codes
- **Numerical stability** and possibility of **large time steps** due to an implicit scheme
- Going further in **quantitative comparison** between the different models and experiments
- In the future : Understand and quantify the **physical origin of basal forces fluctuations**

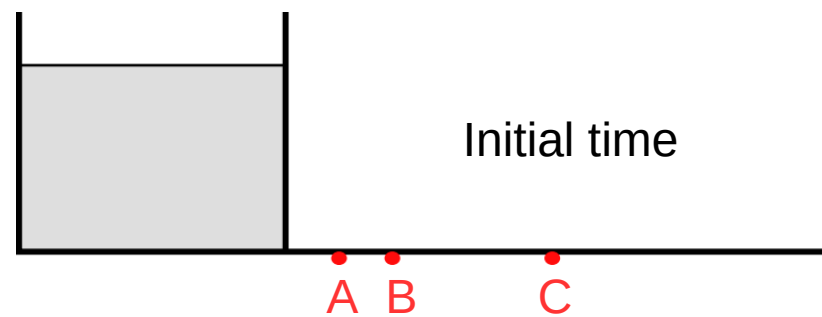




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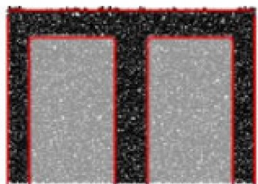
Quantitative comparison with other models and experiments

Comparison **Contact Dynamics**

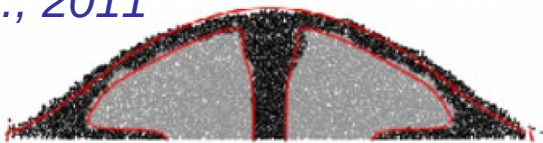
and

Navier-Stokes simulations

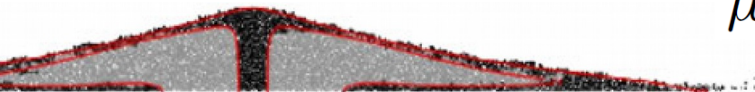
$$\mu = 0.5 \text{ and } e = 0.5$$



$\bar{t} = 0$



$\bar{t} = 1.37$



$\bar{t} = \infty$

Lagree et al., 2011

$$\mu(I) = \mu_s + \frac{\mu_2 - \mu_s}{I_0 + I} I$$

$$\mu_s = 0.32, \Delta\mu = 0.28 \text{ and } I_0 = 0.4$$

Very good agreement **BUT** with parameters smaller than those measured experimentally

$$\mu_s = 0.38, \Delta\mu = 0.26 \text{ and } I_0 = 0.279$$

Jop et al., 2005

DEM goes further than experiments if no additionnal dissipation is accounted for !

Molecular Dynamics & Contact Dynamics

- Molecular Dynamics**

$$m_i \frac{d \mathbf{u}_i}{d t} = m_i \mathbf{g} + \sum_{j=i}^N \mathbf{f}_{i,j}$$

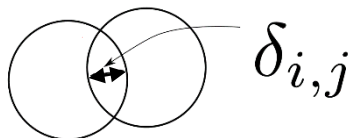
volume
forces

contact
forces

- Contact Dynamics**

Contact forces are functions

Hertz's contact law



normal stiffness

$$\mathbf{f}_{i,j} \cdot \mathbf{n}_{i,j} = \kappa \delta_{i,j}^{\frac{3}{2}}$$

unit normal vector

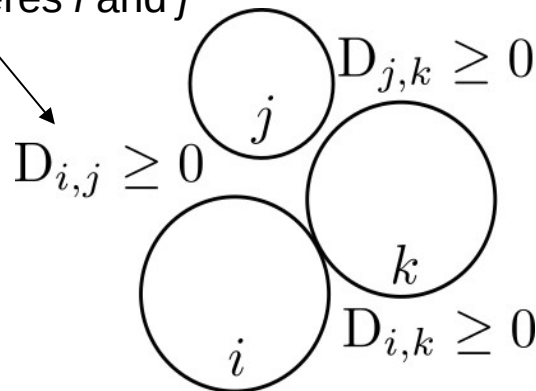
numerical overlap

Constrained optimization problem

Contact forces verify contact laws

Find contact forces such
that beads *do not overlap...*

Distances between
spheres i and j



Larger time steps

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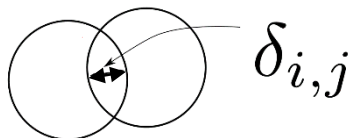
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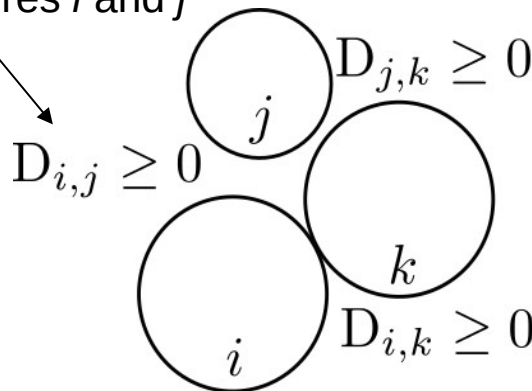
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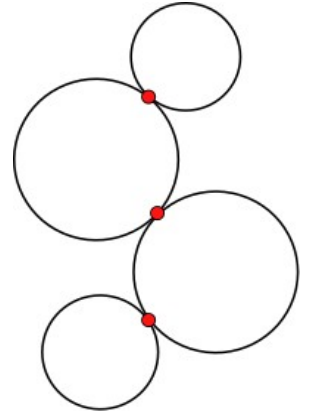
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Global dissipated power of tangential forces



- Convex functional (numerically solved MOSEK)
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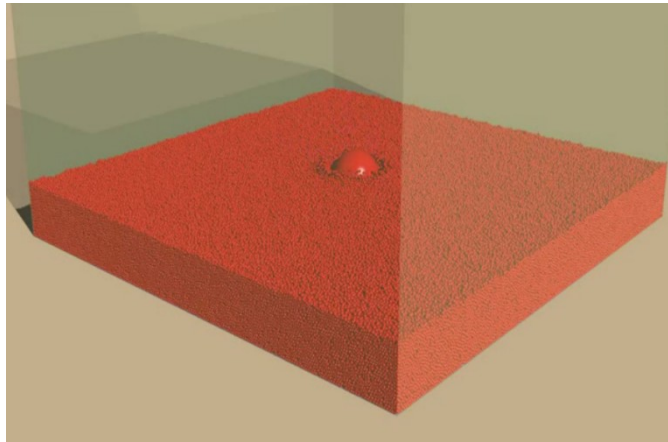
- The choice of the functional implies the prevention of overlaps:

$$D_{i,j}^{n+1} \geq 0 \quad \text{is directly obtained as an optimality condition}$$

Global friction effects in Contact Dynamics

Objective : Numerical scheme dealing with friction
that can handle **large time-step values**

Add friction forces to the global frictionless model **SCoPI**

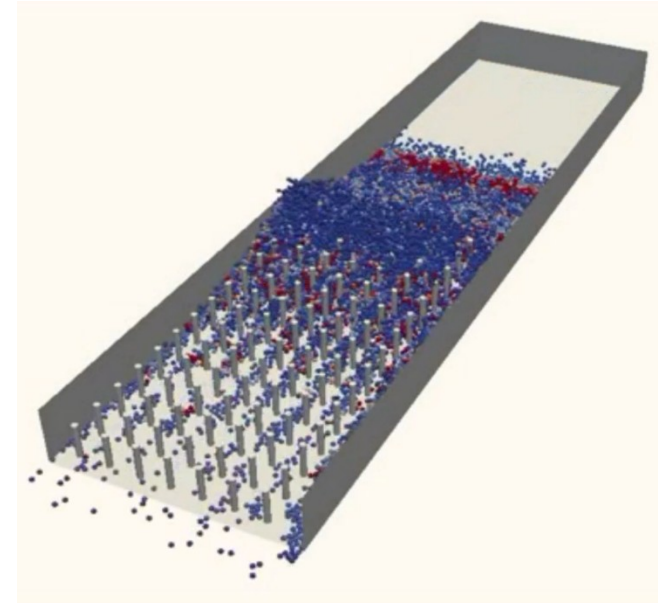
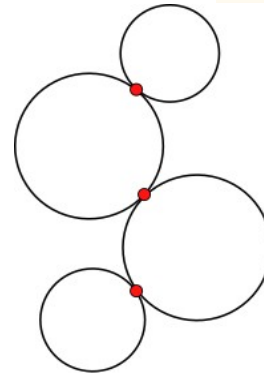


1 000 000 spheres
S. Faure, A. Lefebvre-Lepot

- Global computation of the contact forces at the same time: no iteration

Implicit scheme

Large time steps



40 000 spheres
S. Faure, A. Lefebvre-Lepot

Maury 2006, Lefevre 2009