

Modeling morphological changes by tsunami Induced currents

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Motivation

- Tsunamis have wide-spread and profound effects across the ocean.
- Among those, morphodynamic changes were found in harbor areas where significant strong currents occurred.(e.g., Tsunamiites)
- Tsunami physics in the nearshore area tend to be much complex due to the existence of **turbulence sources**(e.g., bottom boundary layer, wave-breaking).
- Prediction of morphological processes associated with tsunamiinduced currents are highly challenging.



Outlines

Objectives

Develop a numerical solution to predict complex morphodynamic processes in the nearshore.

Strategy

- Set-up modeling tools by integrating sub-module such as
 - Hydrodynamic model
 - Sediment transport model
 - Morphodynamic model
- Finite volume method coupled w/ HLL Riemann solver
- Sensitivity tests on parameters included in closure models

• Scopes

- 1. Model development
- 2. Validations : Dam-break flows, Breaking solitary waves(1D/2D)
- 3. Application

1. Model Development

Model Equations

• Hydrodynamic model : Boussinesq-type equations with rotational terms

Sediment Transport Model

$$\frac{\partial H\overline{c}}{\partial t} + \frac{\partial H\overline{c}\hat{u}_i}{\partial x_i} = \frac{\partial}{\partial x_i} \left(K_h H \frac{\partial \overline{c}}{\partial x_i} \right) + e - d$$

• Morphodynamic Model

$$\frac{\partial h}{\partial t} = \frac{e-d}{1-p}$$

Closures

• Erosion and Deposition Fluxes

$$e = \varphi \left(\theta - \theta_c\right) \left(\overline{u}_i \overline{u}_i\right)^{0.5} H^{-1} (D_{50})^{-0.2} \qquad d = \alpha \overline{c} w_0$$

• Bed-induced Turbulent Eddy Viscosity(Smagorinsky's)

$$\nu_t^h = \left(C_s \Delta x_i\right)^2 \sqrt{2\mathcal{S}_{ij}\mathcal{S}_{ij}}$$

• Wave breaking (Kennedy et al.(2000))

$$R_{i} = \frac{1}{H} \left[\frac{\left(1 + \delta_{ij}\right)}{2} \frac{\partial}{\partial x_{j}} \left\{ \nu_{b} \frac{\partial \left(H \hat{u}_{i}\right)}{\partial x_{j}} \right\} + \frac{\left|\epsilon_{ij}\right|}{2} \frac{\partial}{\partial x_{j}} \left\{ \nu_{b} \frac{\partial \left(H \hat{u}_{j}\right)}{\partial x_{i}} \right\} \right]$$

• Turbulence Backscattering Model(Hinterberger et al.(2007))

$$F_i = C_b \frac{\sqrt{\hat{u}_j \hat{u}_j}}{H} \sqrt{\frac{\nu \sqrt{C_f}}{\Delta t}} r_i$$

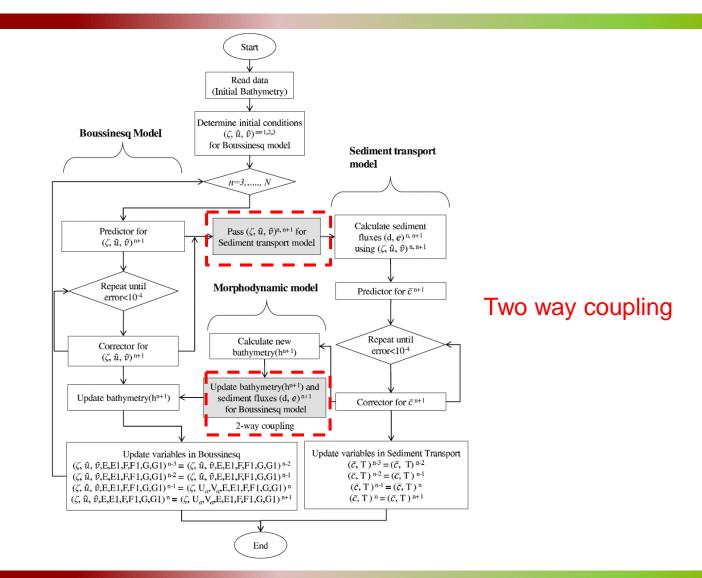
Numerical Methods

• Leading order terms :

- 4th order MUSCL-TVD scheme by Yamamoto & Daiguji(1993) incorporated with approximated HLL Riemann Solver

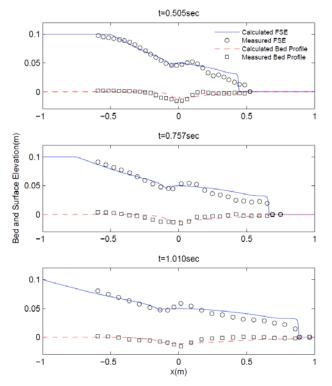
- Higher order terms :
 - Cell-centered Finite Volume Method by Lacor(2004)
- Time marching :
 - 3rd order Adams-Bashforth predictor and
 - 4th order Adams-Moulton corrector

Flow Chart

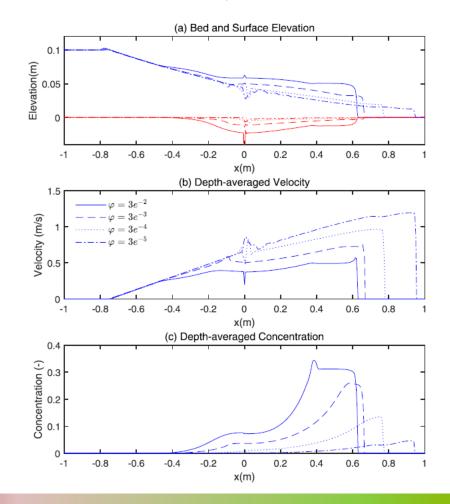


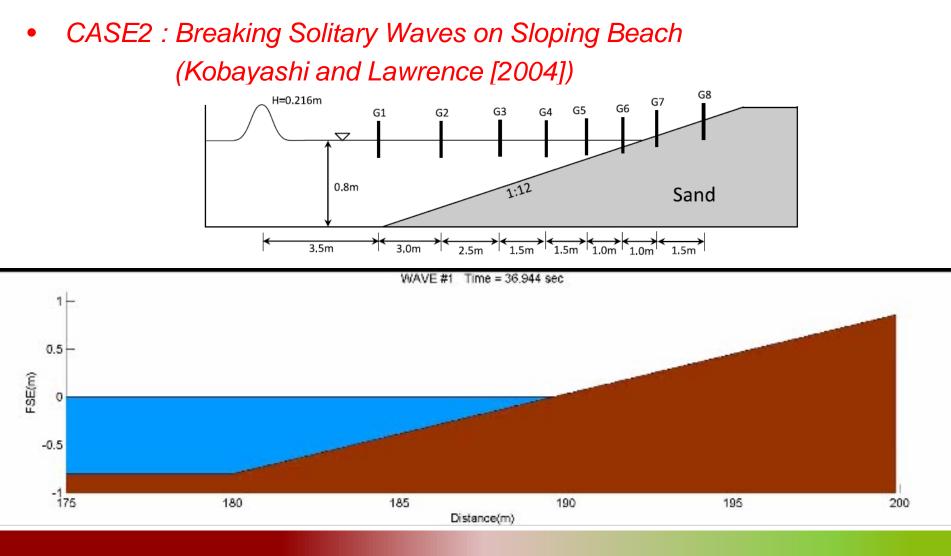
2. Model Validations

• CASE1 : 1D Dam Breaking over a Movable Bed (Fraccarollo and Capart [2002])

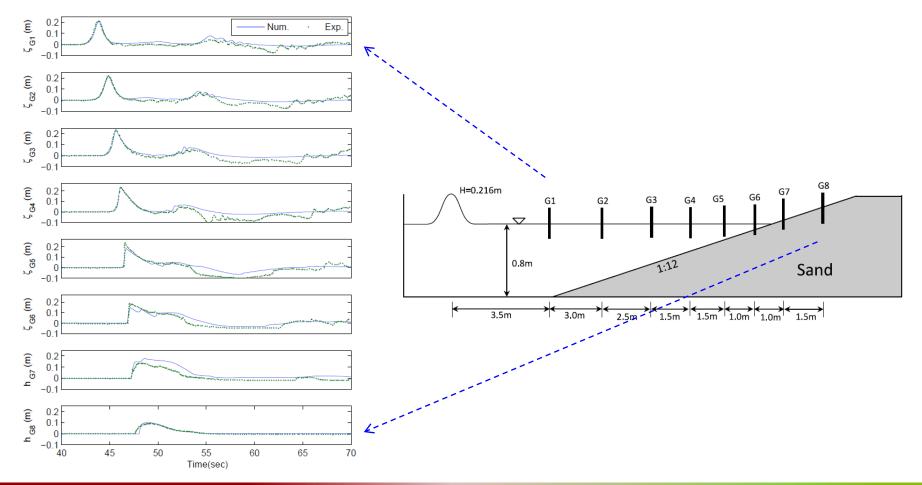


Sensitivity tests on φ

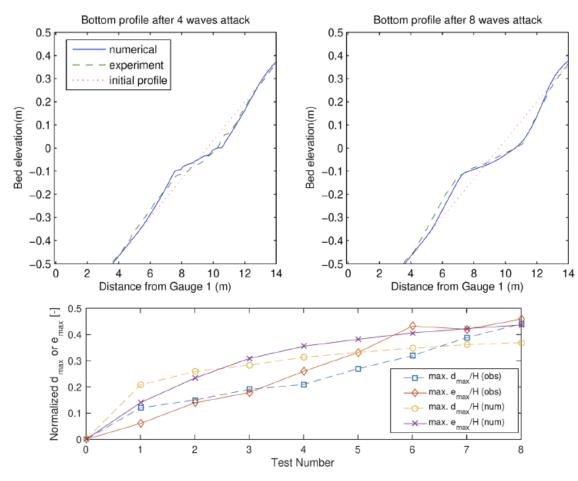




CASE2 : Breaking Solitary Waves on Sloping Beach

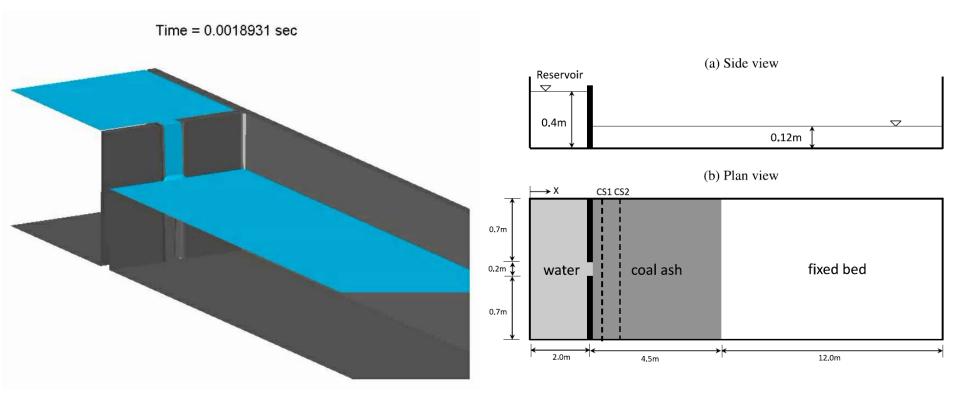


• CASE2 : Breaking Solitary Waves on Sloping Beach

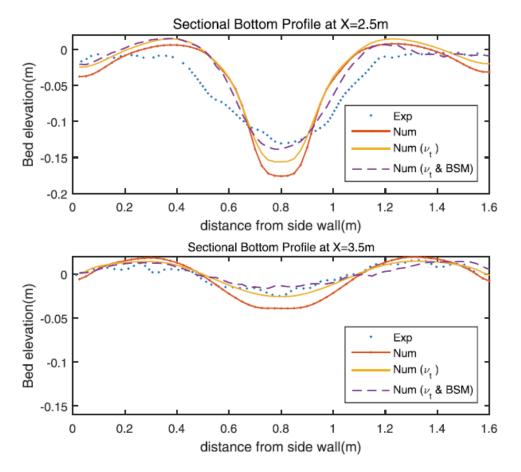


A significant erosion process at the foreshore may be explained by the strong backwash current initiated when a solitary wave retreats.

• CASE3 : Dam-Break Flow through a Partial Breach

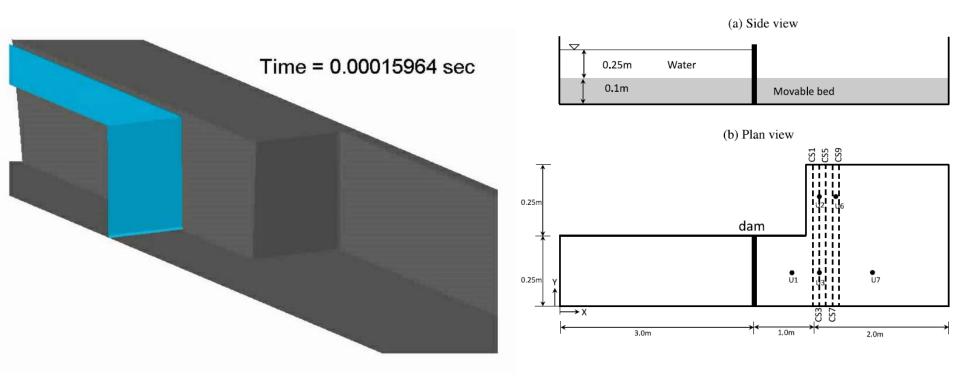


• CASE3 : Dam-Break Flow through a Partial Breach

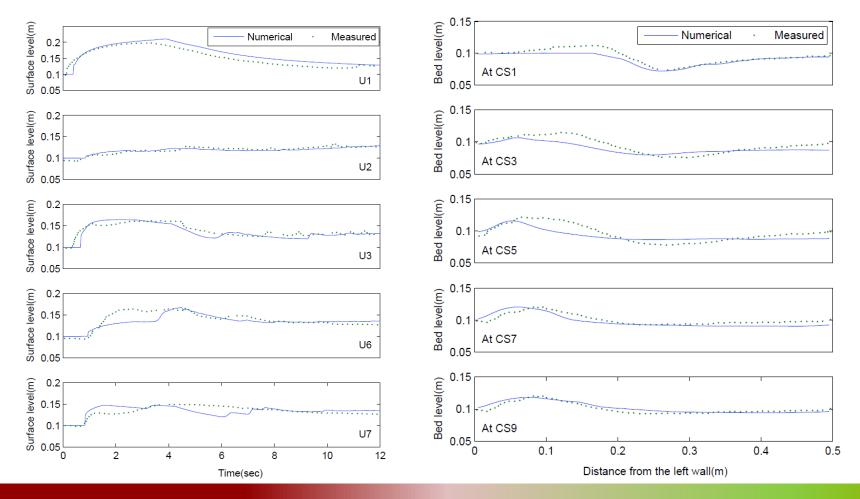


Reasonable agreement found when including turbulence effects, while the calculations overestimated the peak erosion depth at CS1.

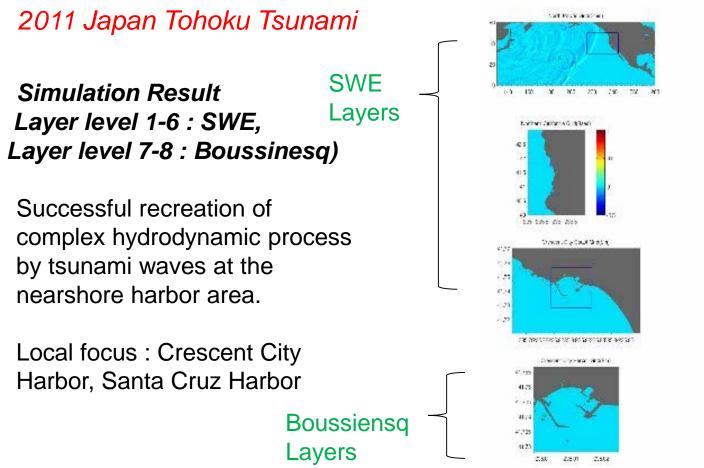
• CASE4 : Dam-Break Flow over a Movable Bed Channel with Sudden Enlargement



• CASE4 : Dam-Break Flow over a Movable Bed Channel



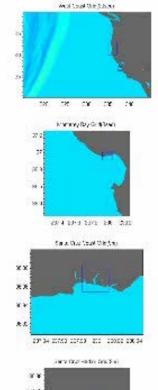
3. Model Applications

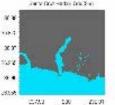


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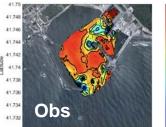
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Time = 480min

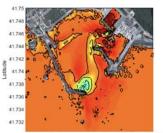




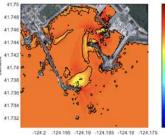
Crescent City Harbor •



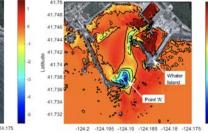
-124.2 -124.195 -124.19 -124.185 -124.18 -124.175 Longitude



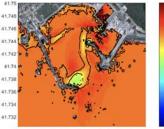
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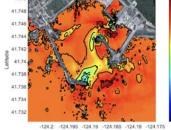
Longitude



Longitude

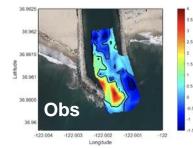


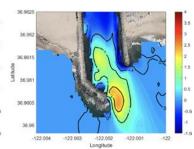
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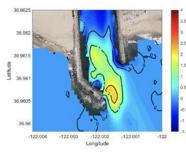


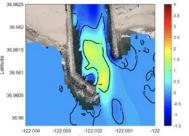
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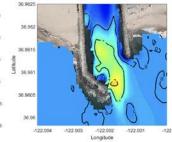
Santa Cruz Harbor

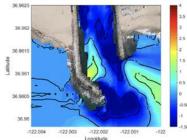


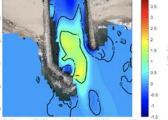








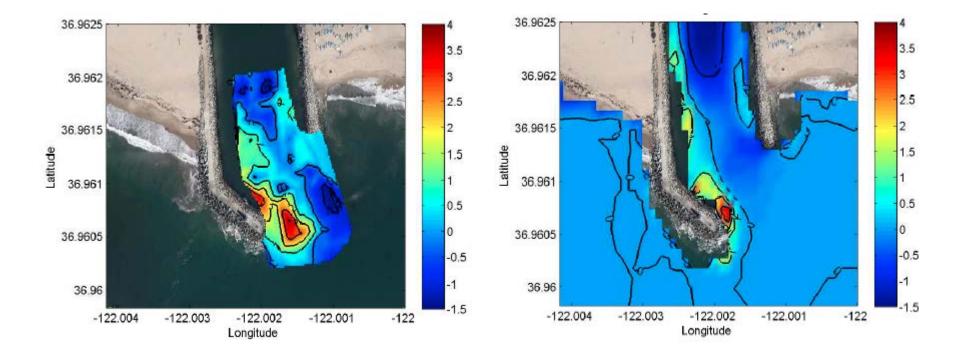






Applications

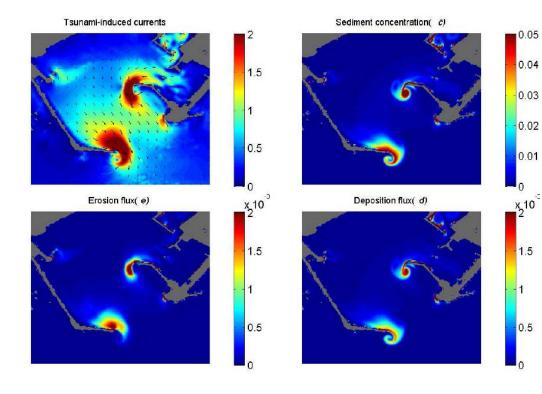
• Santa Cruz Harbor



Observed data (Wilson et al.(2012))

Modeled results

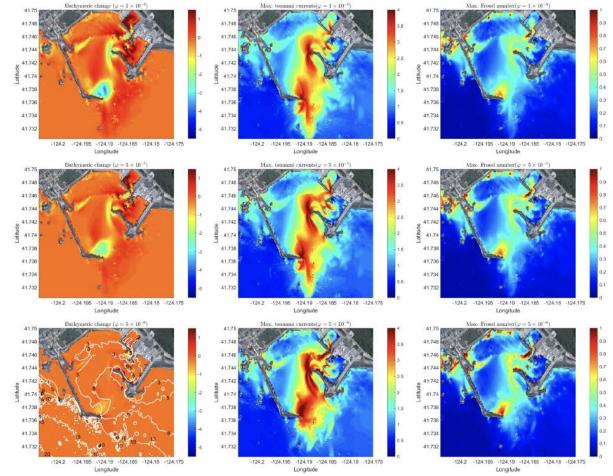
 Numerical results of bathymetric changes in Crescent City Harbor at time t = 637 min since EQ.



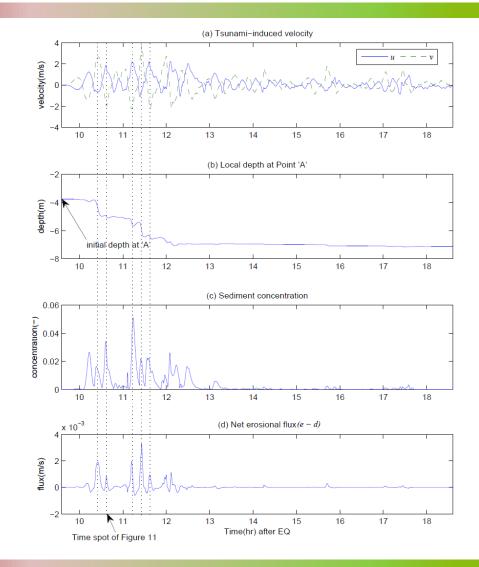


Very active sedimentation processes in the vicinity of the outer and inner harbour entrances

- Sensitivity tests on φ show that smaller φ produced less erosive sedimentation process
- Tsunami momentum is damped due to the strong interaction between surface processes and landforms, so the propagation gets retarded.



- Calculated time history at local point 'A'
 - (a) velocity
 - (b) local depth
 - (c) sediment concentration
 - (d) net erosion flux
- Coastal morphologic evolution is significant during the initial 3–4 hrs.
- Physics of tsunami-induced sedimentation is confined to a time scale of O(hours).





- 1. A numerical model to predict morphologic changes by tsunamiinduced current is developed by coupling 'hydrodynamicmorphologic models.
- 2. The model is validated through 1D and 2D sediment problems, with a comprehensive test on prametric sensitivity.
- 3. Application to the real tsunami event(2011 Japan Tohoku Tsunami) revealed that

"the simulated bathymetric changes provide good approximations to the observation as long as the parameters is properly chosen"