

## 1. Motivation

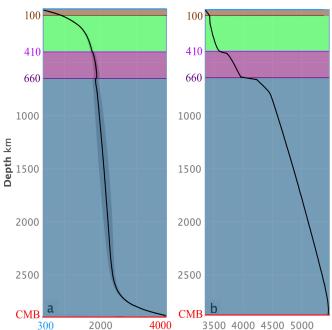
In numerical simulations four types of lid regimes can be obtained by varying the **yield strength**.  
Also numerical parameters, such as the **grid resolution**, determines the outcome of a simulation.

**Guiding question:** What is the effect of grid resolution on the tectonic regime?



## 4. Model Assumptions

- Isothermal, free slip boundaries
- Constant radiogenic heating
- No melting
- Composition: 60% ol + 40% pxgt
- Exothermic phase change (Wd)
- Endothermic phase change (Pv)
- Upper/lower  $\eta$  cutoff:  $10^{28}/10^{17}$  Pa s
- 15 Gyrs simulated time
- Initial Rayleigh Number:  $8 \times 10^7$
- Constant yield strength



## 3. Rheology

- Arrhenius law: strongly **T-dependent** viscosity ( $\eta_{\text{diff}}$ )

$$\eta_{\text{diff}}(T, P) = \eta_0 \exp\left(\frac{E+PV}{RT} - \frac{E}{RT_0}\right)$$

- Plastic rheology: **Yield Stress limiter** ( $\tau_y$ ) restricts  $\eta_{\text{app}}$

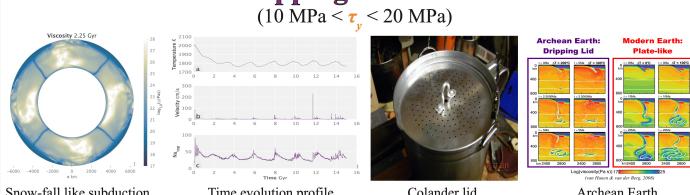
$$\eta_{\text{app}} = \frac{\tau_y}{2\dot{\epsilon}_{II}}$$

- Effective viscosity: minimum between  $\eta_{\text{diff}}$  and  $\eta_{\text{app}}$

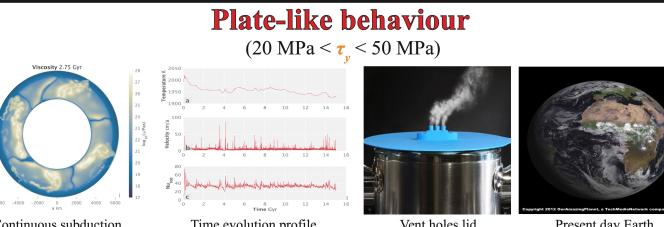
$$\eta_{\text{eff}} = \min[\eta_{\text{diff}}(T, P), \eta_{\text{app}}(\tau_y, \dot{\epsilon}_{II})]$$

## 5. Lid Regimes

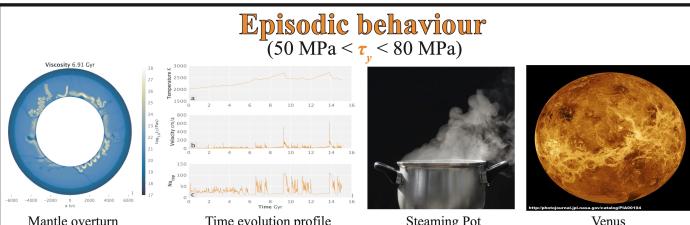
### Dripping behaviour (10 MPa < $\tau_y$ < 20 MPa)



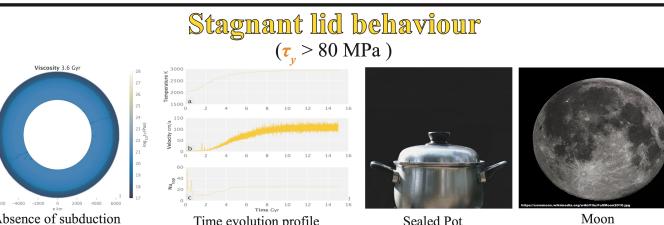
### Plate-like behaviour (20 MPa < $\tau_y$ < 50 MPa)



### Episodic behaviour (50 MPa < $\tau_y$ < 80 MPa)



### Stagnant lid behaviour ( $\tau_y$ > 80 MPa)



## 8. Conclusions

- Yield strength** controls the strength of the lithosphere leading to 4 different behaviours:  
**Dripping, Plate-like, Episodic, Stagnant**
- Grid resolution** is a key numerical parameter since it affects the lid behaviour stability domain
- Critical  $\tau_y$  that separates plate-like from episodic regime shifts toward higher  $\tau_y$ , either if the **radial resolution** is low or the **azimuthal** is high

## 2. StagYY

- Code **StagYY** (1), data analysis **StagLab** (2)
- Spherical annulus geometry (3), equatorial slice of a planet

### Azimuthal resolution ( $\phi$ )

in the  $y$  direction (longitude)

### Radial resolution ( $r$ )

in the  $z$  direction (radius)

### Zenithal resolution ( $\theta$ )

in the  $x$  direction (latitude)

- Stokes equations solved for compressible material:

### Continuity Equation

$$\frac{\partial \rho}{\partial t} + \frac{1}{r^d} \frac{\partial}{\partial r} (r^d \rho v_r) + \frac{\partial}{\partial \phi} [\rho (\frac{v_\phi}{r})] = 0 \quad \frac{1}{r^d} \frac{\partial}{\partial r} (r^d \tau_{rr}) + \frac{1}{r} \frac{\partial \tau_{r\phi}}{\partial \phi} - \frac{\tau_{\phi\phi} + \tau_{\theta\theta}}{r} - \frac{\partial p}{\partial r} - \rho g = 0$$

### Energy Equation

$$\frac{1}{r^d} \frac{\partial}{\partial r} (r^d \tau_{\phi\phi}) + \frac{1}{r} \frac{\partial \tau_{\theta\theta}}{\partial \phi} + \frac{\tau_{r\phi}}{r} - \frac{1}{r} \frac{\partial p}{\partial \phi} = 0 \quad \frac{\partial e}{\partial t} + v_r \frac{\partial e}{\partial r} + (\frac{v_\phi}{r}) \frac{\partial e}{\partial \phi} = \frac{1}{r^d} \frac{\partial}{\partial r} (r^d K \frac{\partial T}{\partial r}) + \frac{1}{r^2} \frac{\partial}{\partial \phi} (K \frac{\partial T}{\partial \phi}) + H$$

### Angular Component of Momentum Equation

$$\frac{1}{r^d} \frac{\partial}{\partial r} (r^d \tau_{r\phi}) + \frac{1}{r} \frac{\partial \tau_{\theta\theta}}{\partial \phi} + \frac{\tau_{r\phi}}{r} - \frac{1}{r} \frac{\partial p}{\partial \phi} = 0 \quad \frac{\partial e}{\partial t} + v_r \frac{\partial e}{\partial r} + (\frac{v_\phi}{r}) \frac{\partial e}{\partial \phi} = \frac{1}{r^d} \frac{\partial}{\partial r} (r^d K \frac{\partial T}{\partial r}) + \frac{1}{r^2} \frac{\partial}{\partial \phi} (K \frac{\partial T}{\partial \phi}) + H$$

### Radial Component of Momentum Equation

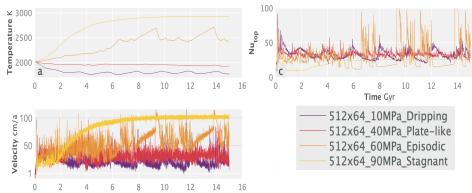
$$\frac{1}{r^d} \frac{\partial}{\partial r} (r^d \tau_{rr}) + \frac{1}{r} \frac{\partial \tau_{r\phi}}{\partial \phi} - \frac{\tau_{\phi\phi} + \tau_{\theta\theta}}{r} - \frac{\partial p}{\partial r} - \rho g = 0 \quad \frac{\partial e}{\partial t} + v_r \frac{\partial e}{\partial r} + (\frac{v_\phi}{r}) \frac{\partial e}{\partial \phi} = \frac{1}{r^d} \frac{\partial}{\partial r} (r^d K \frac{\partial T}{\partial r}) + \frac{1}{r^2} \frac{\partial}{\partial \phi} (K \frac{\partial T}{\partial \phi}) + H$$

## 6. Nusselt Number

A very useful parameter to study the different lid behaviours

$$Nu = \frac{q_{\text{tot}}}{q_{\text{cond}}} = \frac{\text{total heat transport}}{\text{conductive heat transport}}$$

## 7. Resolution Tests



Different lid regimes can be distinguished by:

- Temperature profile
- Surface Nusselt number
- Average velocity profile

12 different **grid resolutions** (from **128x32** up to **1024x128**) over a range of 9 different  $\tau_y$  (from 10 to 90 MPa)

