

# Fast Analytical Models for Texture Evolution in Anisotropic Polycrystals



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## *Collaborators:*

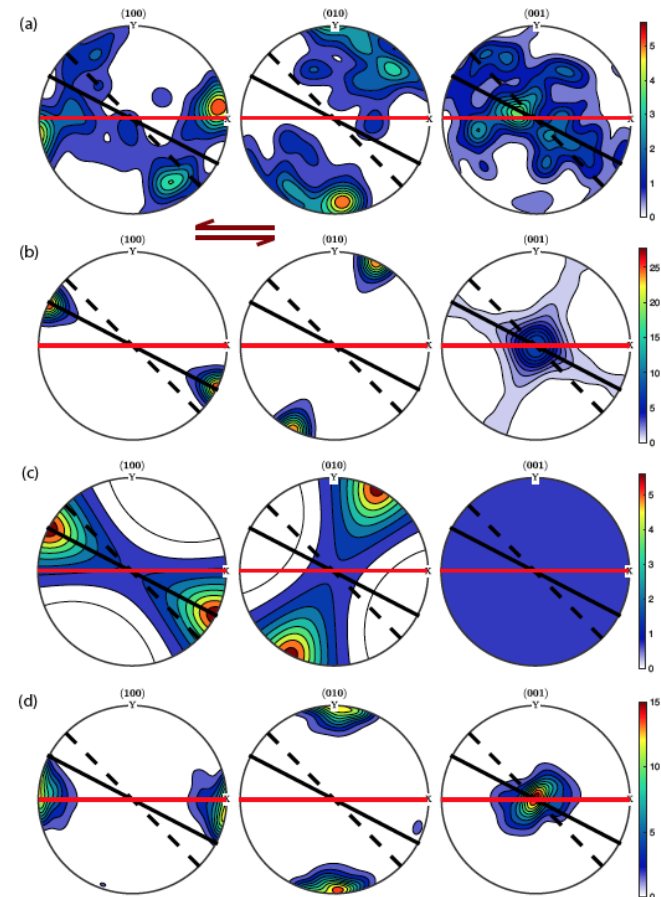
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**James WOOKEY (Bristol)**



# Aim

*Context:* To predict seismic anisotropy from geodynamical models, we need to be able to calculate how crystal preferred orientation (CPO) evolves during progressive deformation

*Difficulty:* Self-consistent models (VPSC, SOSC) are too computationally expensive to include in 3-D convection codes

*This work:*

Design faster algorithms based on:

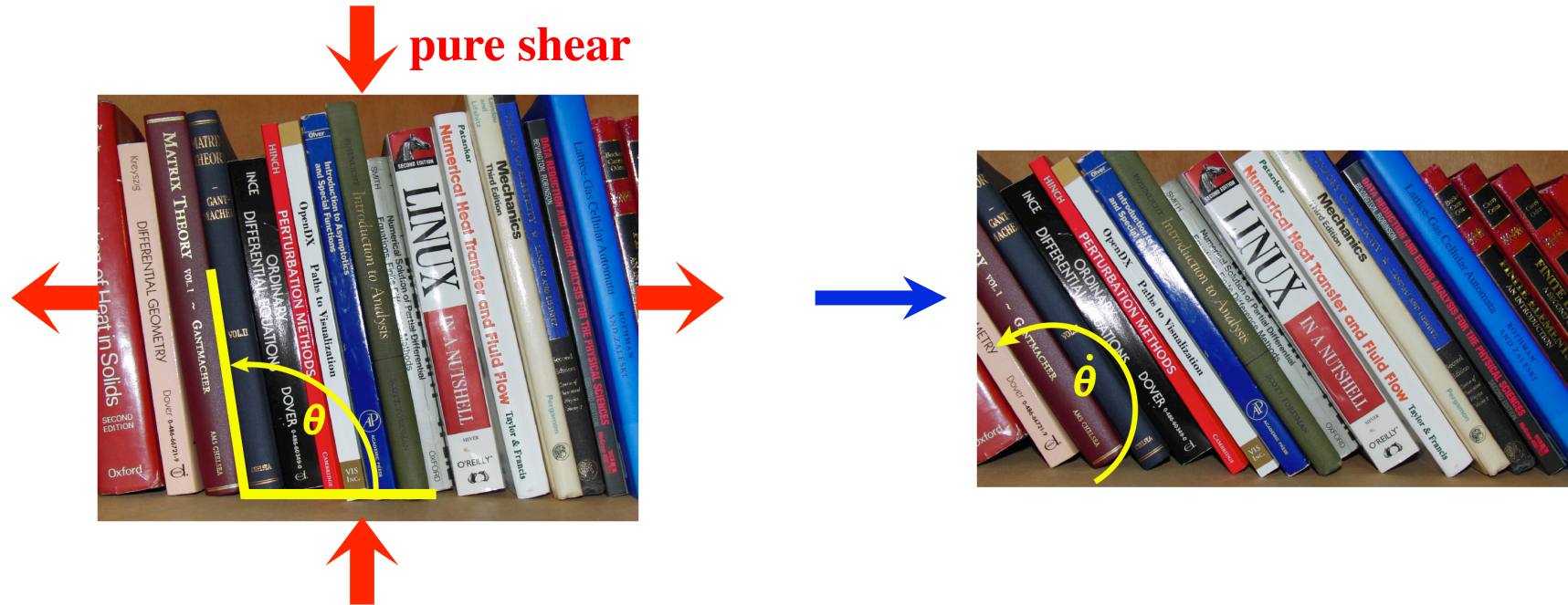
- an analytical expression for crystallographic spin ➡ model ANPAR
- an economical analytical representation of CPO in terms of « structured basis functions » ➡ model SBFTEX



Photo: Tim Walker



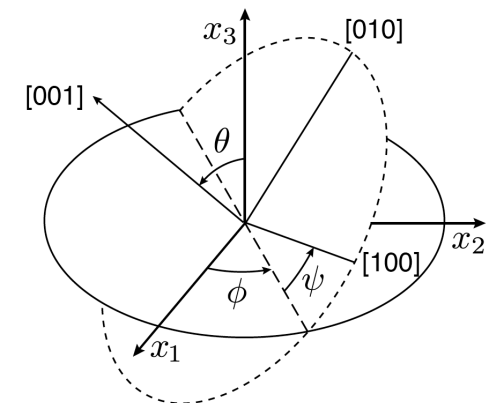
# Mechanism of crystallographic rotation



## Generalization to 3-D:

**Orientation :** three Eulerian angles  $(\phi, \theta, \psi) \equiv \mathbf{g}$

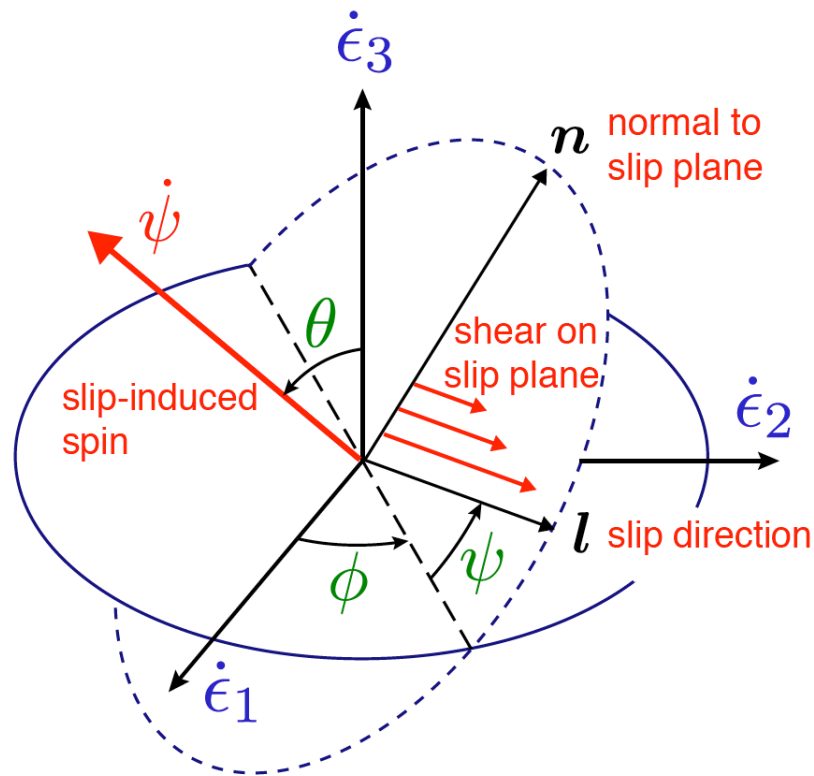
**Spin :**  $(\dot{\phi}, \dot{\theta}, \dot{\psi}) \equiv \dot{\mathbf{g}}$



# Analytical expression for crystallographic spin

**Model:** aggregate of crystals with one active slip system, deformed by triaxial straining

(principal strain rates  $\dot{\epsilon}_1, \dot{\epsilon}_2, \dot{\epsilon}_3$ )



Minimize difference of crystal and aggregate deformation rates  $\longrightarrow$

$$\dot{\psi} = A \left\{ \frac{3}{4} \dot{\epsilon}_3 \sin 2\psi \sin^2 \theta + \frac{1}{8} (\dot{\epsilon}_2 - \dot{\epsilon}_1) [4 \sin 2\phi \cos \theta \cos 2\psi + \cos 2\phi (\cos 2\theta + 3) \sin 2\psi] \right\}$$

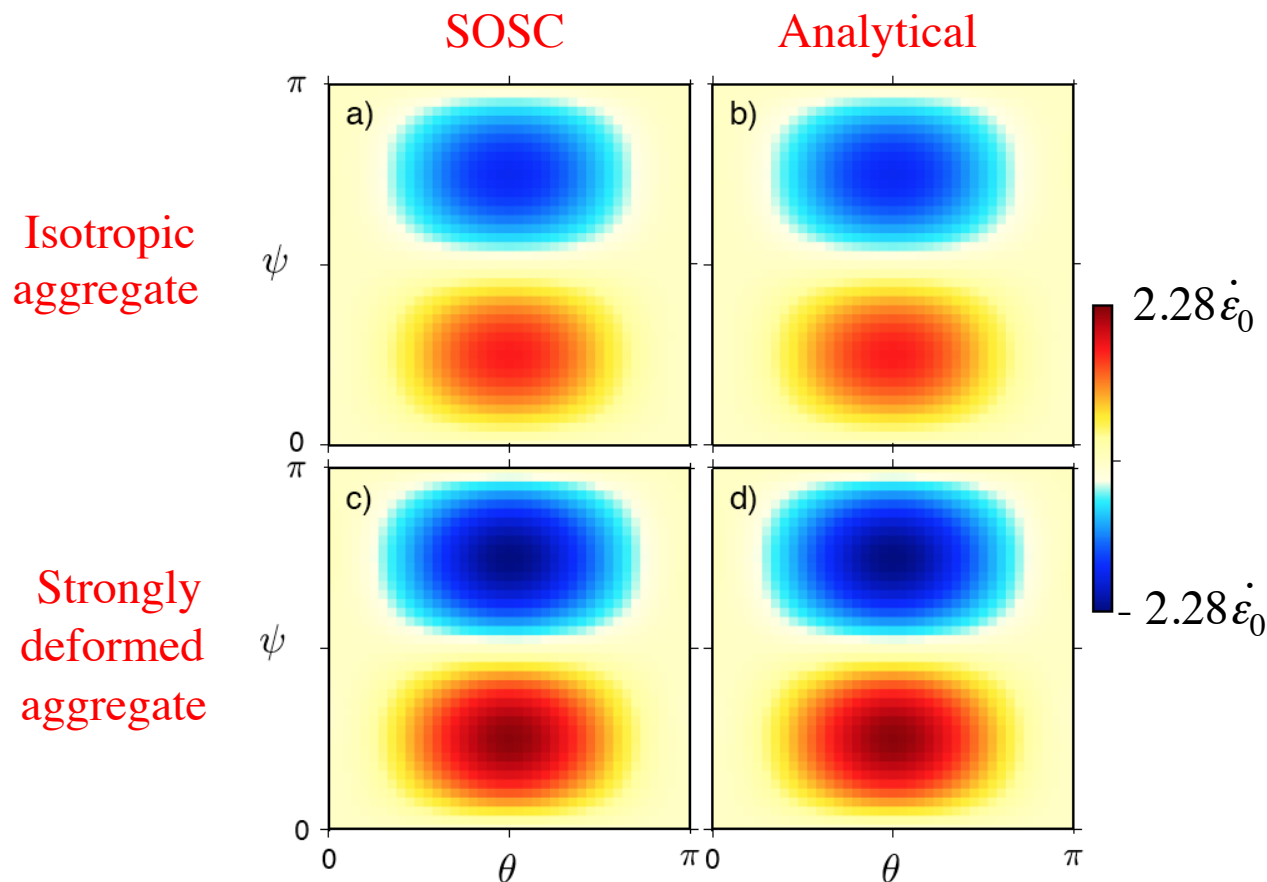
**Amplitude A:**

- = 5 if global strain rate compatibility is enforced
- = 1 if not enforced
- = intermediate if several slip systems are active

# Analytical expression for the spin: Validation against SOSC

*Test case:* uniaxial compression (shortening rate  $\dot{\epsilon}_0$ )

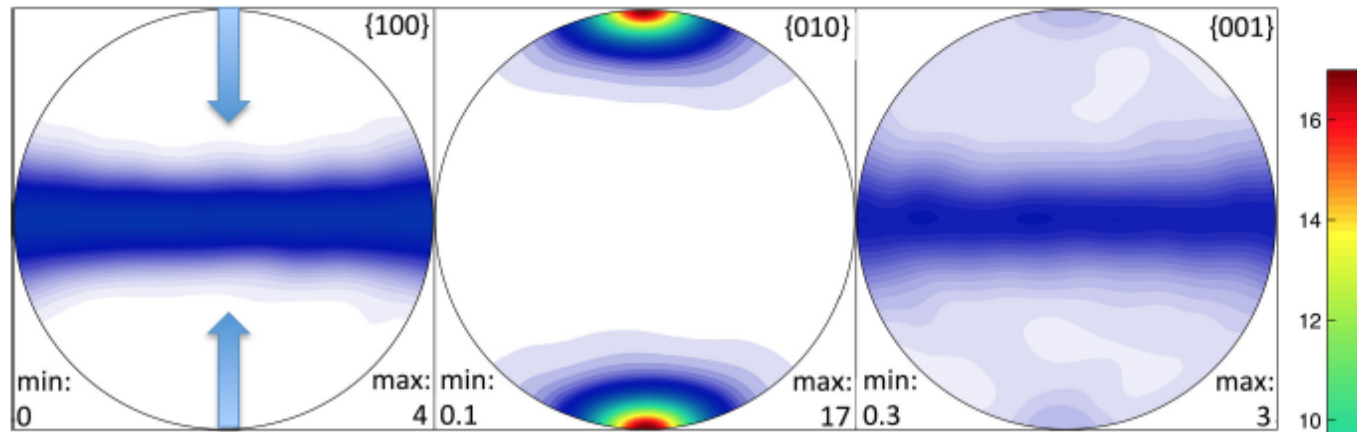
*Quantity shown:* spin  $\dot{\psi}$  for slip system (010)[100] of olivine



The analytical model reproduces *exactly* the orientation-dependence of crystal spin predicted by the SOSC model

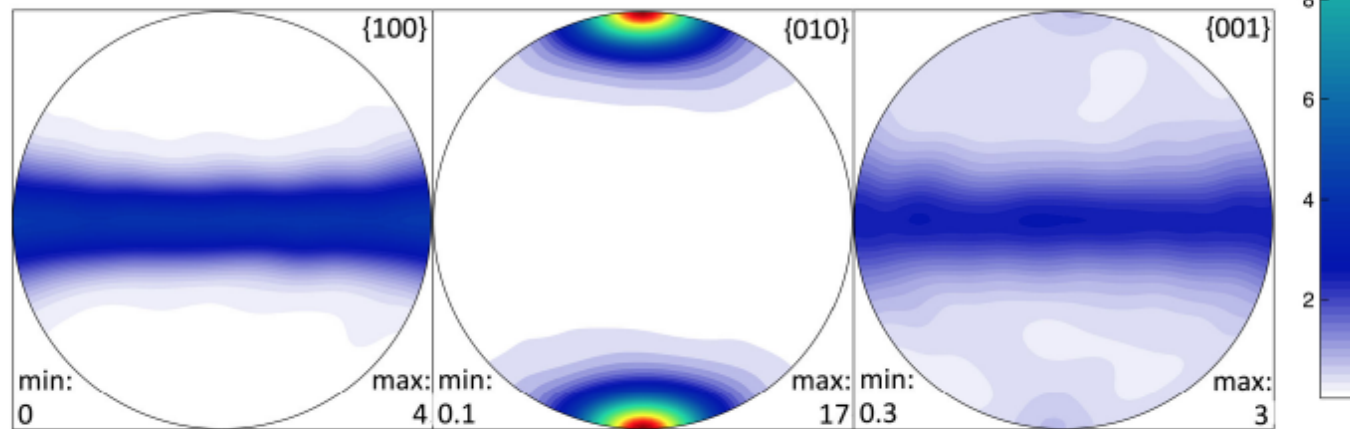
# ANPAR vs. SOSC: Uniaxial compression (45% shortening) of an olivine polycrystal

SOSC



(a) SO model.

ANPAR



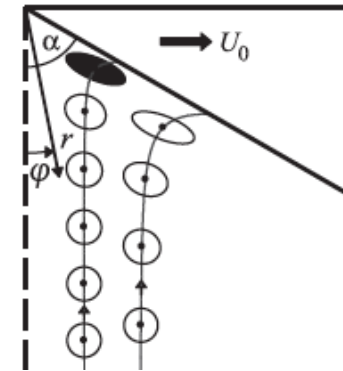
(b) ANPAR

multiples  
of random  
distribution

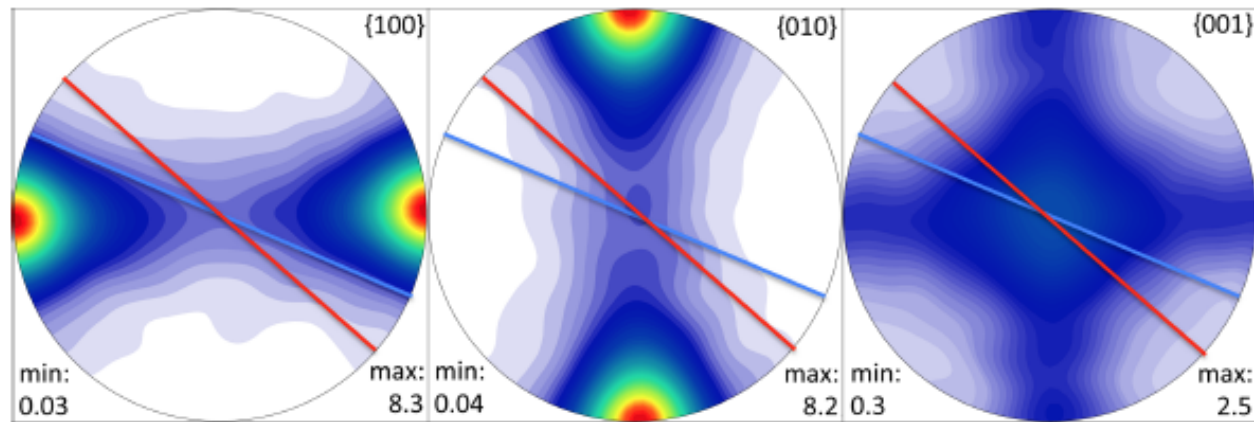


# ANPAR vs. SOSC: Corner Flow Model

- long finite strain axis
- shear plane

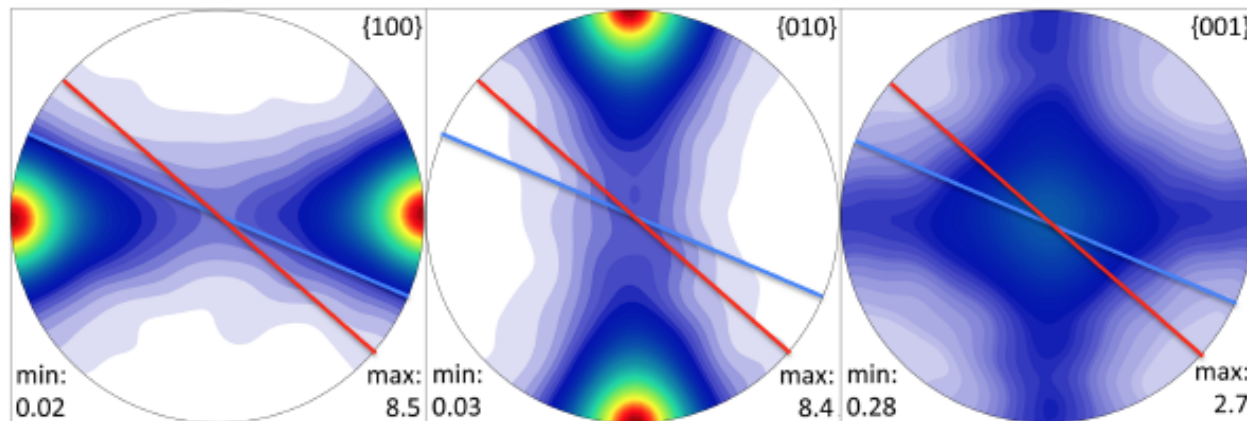


SOSC



(a) SO model.

ANPAR



multiples  
of random  
distribution

## Analytical description of CPO

*Idea* : represent CPO using « structured basis functions » that:

- satisfy automatically the symmetry of the imposed deformation
- can represent arbitrarily sharp textures
- are analytical solutions of the evolution equation for the ODF:

$$\frac{\partial f}{\partial t} + \nabla \cdot (\dot{\mathbf{g}} f) = 0$$



Number of SBFs required  
= Number of active slip systems



## Structured basis functions

**General form** (for time-independent spin amplitude  $A$ ):

$$f = f(\underbrace{\phi, \theta, \psi}_{\text{Eulerian angles}}, \underbrace{A}_{\text{spin amplitude}}, \underbrace{c_1/c_2, c_2/c_3}_{\text{finite strains}})$$

**Exact expression:**

$$f = f_0 [\cosh A\Gamma - \sin 2(\psi - \chi) \sinh A\Gamma]^{-1}$$

$$\Gamma = [r_{12}^2 F^2 + (r_{12}G + r_{23}H)^2]^{1/2}$$

$$\{\cos 2\chi, \sin 2\chi\} = \Gamma^{-1} \{r_{12}F, r_{12}G + r_{23}H\} \quad r_{ij} = \ln(c_i/c_j)$$

$$F = -\sin 2\phi \cos \theta \quad H = -\sin^2 \theta$$

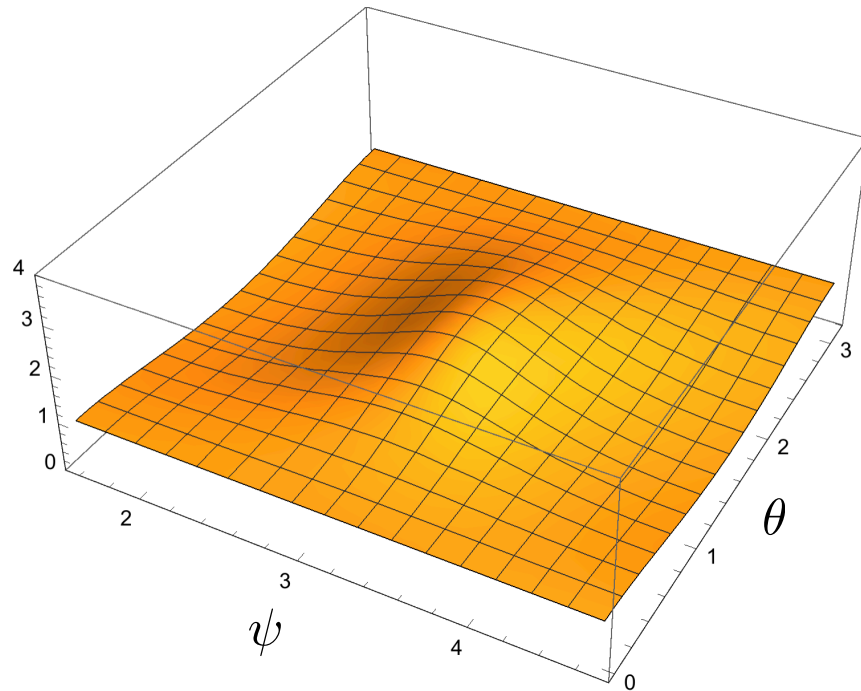
$$G = \sin^2 \phi \cos^2 \theta - \cos^2 \phi$$

**Interpretation:**

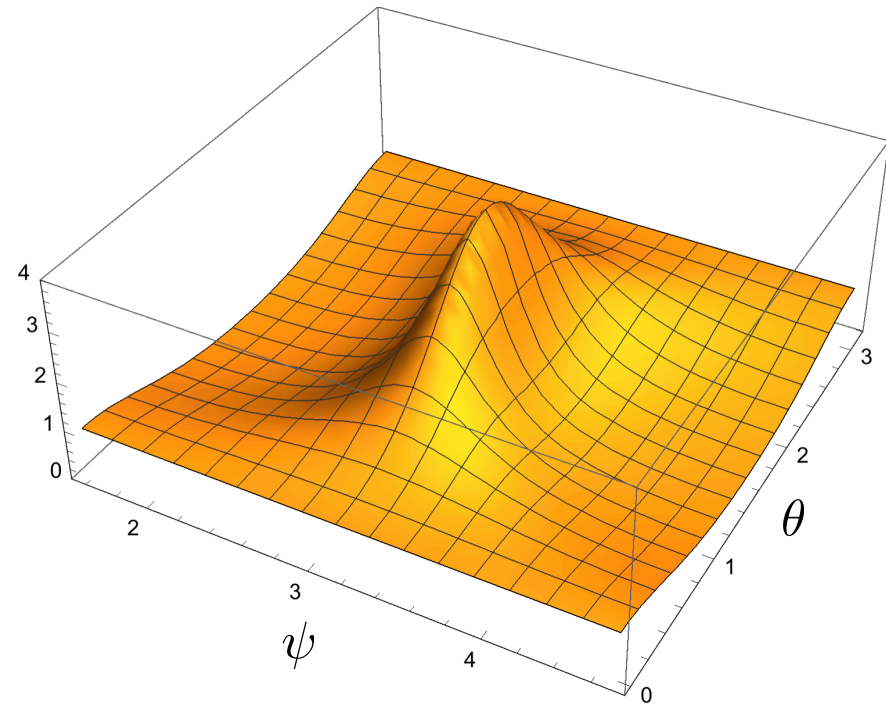
SBF = virtual CPO produced by the action of a single slip system

## Structured basis function vs. strain (uniaxial compression)

30% shortening



60% shortening



SBF automatically gets sharper as strain increases

## SBF expansion of the orientation distribution function

$$\mathcal{F}(\mathbf{g}) = \underbrace{1}_{\text{isotropic part}} + \sum_{s=1}^3 \underbrace{C_s(p_{12}, p_{23}, r_{12}, r_{23})}_{\text{precalculated expansion coefficients}} \underbrace{[f(\mathbf{M}_s \mathbf{g}, r_{12}, r_{23}) - 1]}_{\text{anisotropic part of SBF for slip system } s}$$

ODF

$$p_{ij} = \ln \frac{\tau_i}{\tau_j} \quad (\text{relative strengths of slip systems})$$

$$r_{ij} = \ln \frac{c_i}{c_j} \quad (\text{axial ratios of finite strain ellipsoid})$$

$$\mathbf{M}_s = \text{rotation matrix for slip system } s$$



Given the finite strain and the slip system strengths,  
the full ODF can be calculated

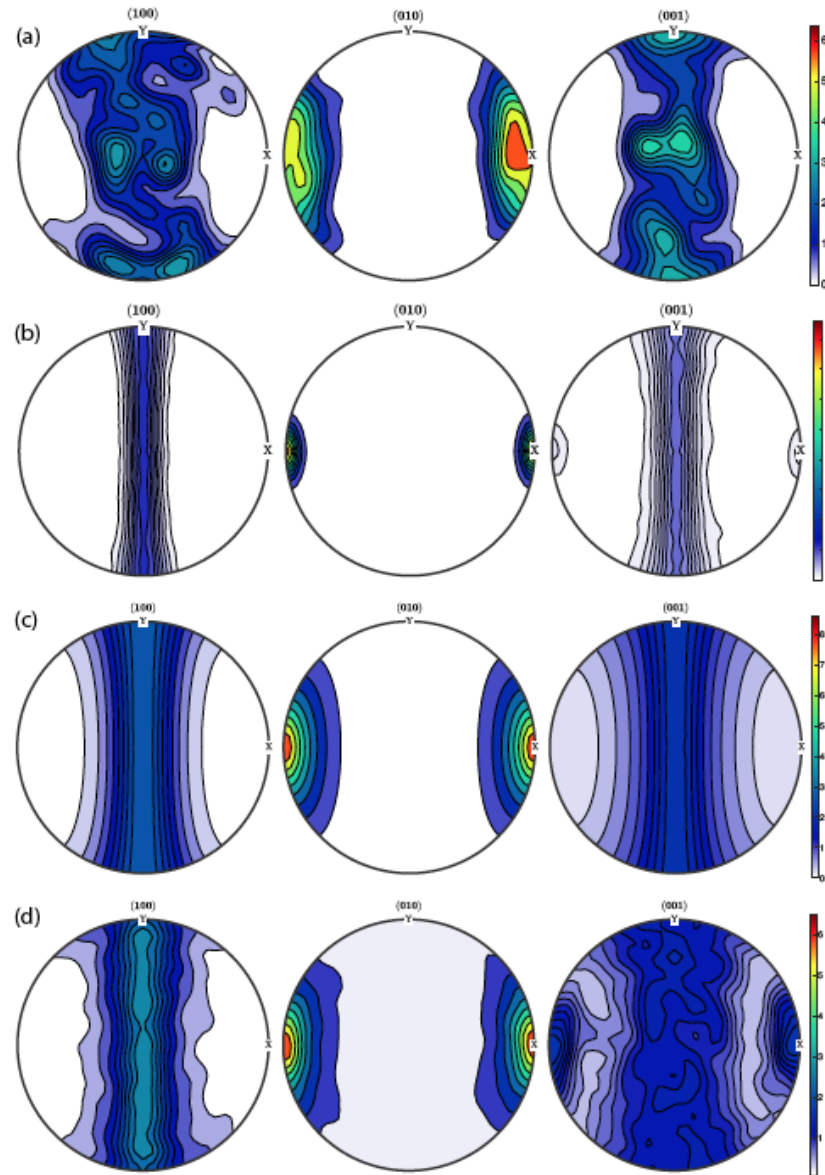
# SBFTEX prediction: Uniaxial compression (58% shortening)

Laboratory experiment  
(Nicolas et al. 1973)

SOSC

SBFTEX

D-Rex



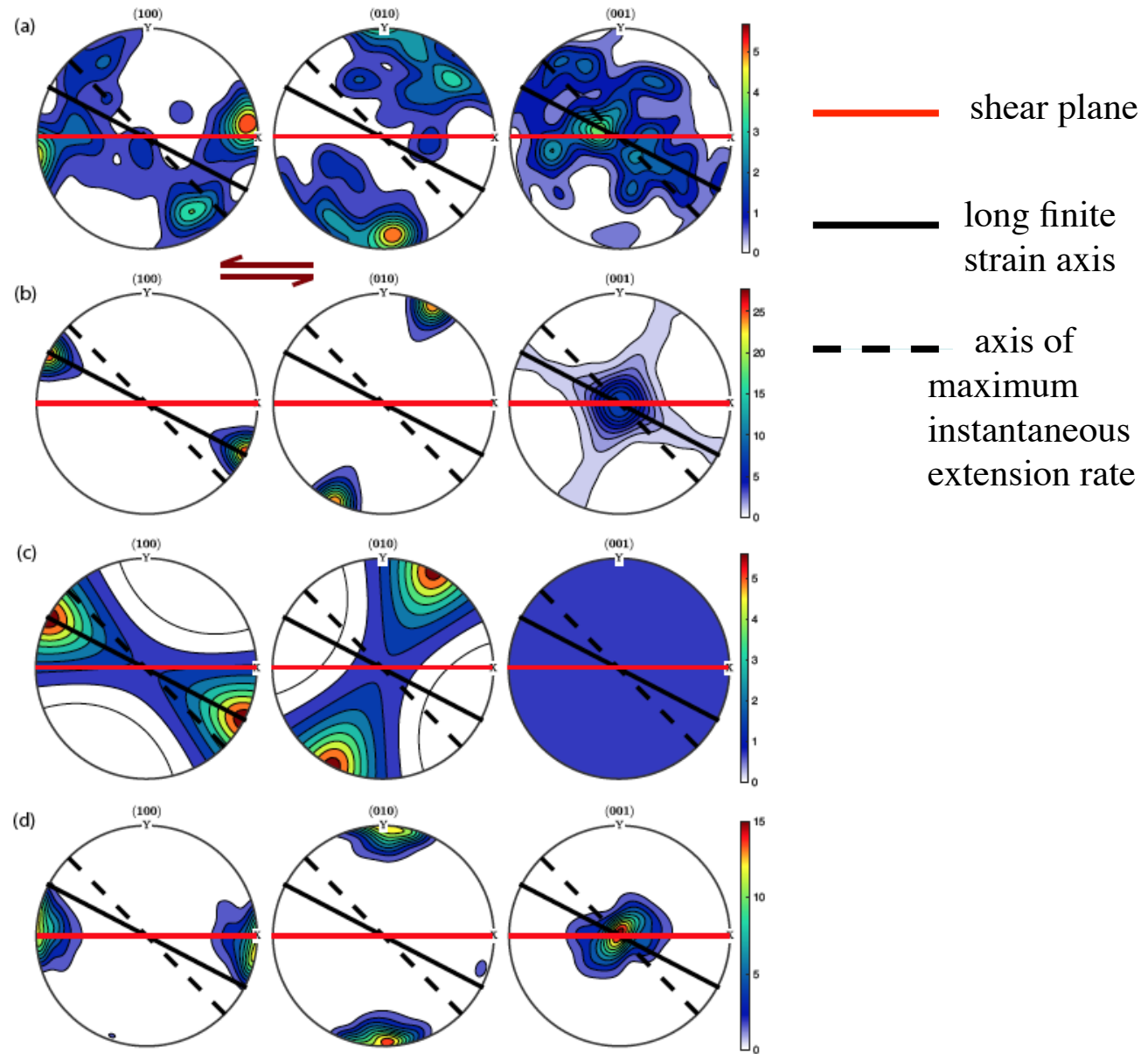
# SBFTEX prediction: Simple shear ( $\gamma = 140\%$ )

Laboratory experiment  
(Lee et al. 2002)

SOSC

SBFTEX

D-Rex



# Summary and Perspectives

## *Advantages of the structured basis function approach:*

- ☞ Representation of CPO is
  - ◆ smooth (uses continuous functions)
  - ◆ economical (typically 3 coefficients)
- ☞ Expression for crystallographic spin agrees exactly with the SOSC model
- ☞ Calculations are  $\sim 10^7$  times faster than SOSC
- ☞ Can be applied to both upper- and lower-mantle phases

## *Future work:*

- ☞ extension to two-phase aggregates
- ☞ parameterization of recrystallization
- ☞ user-friendly open-source implementation





