

Street canyon ventilation: Combined effect of cross-section geometry and wall heating

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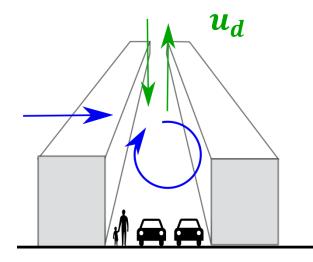
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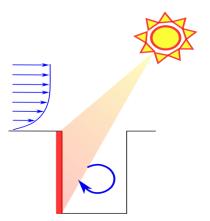
POLITECNICO DI TORINO

Dipartimento di Ingegneria dell'Ambiente, del Territorio e delle Infrastrutture Introduction



The vertical velocity of mass transfer of pollutants (u_d) is a function of:

- EXTERNAL FLOW
- ASPECT RATIO (H/W)
- WALL ROUGHNESS
- WALL HEATING (ΔT)
 - OBSTACLES (trees)

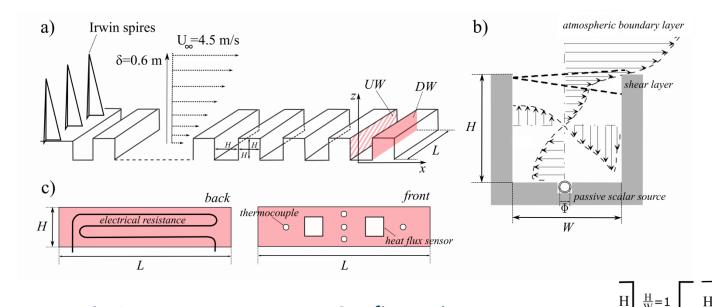


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Wind-tunnel experiments to investigate the physical mechanisms that govern the vertical transfer of pollutants (u_d) from a canyon to the overlying atmosphere

The experimental set-up



Measurement techniques

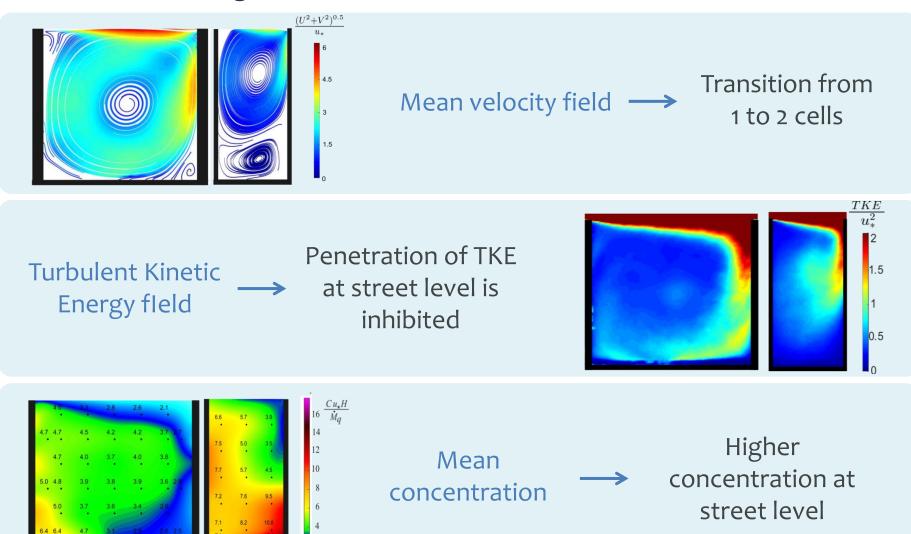
- Configurations
- Thermal fluxes at walls → heat flux sensors Different geometries (H/W)
- **Temperature** at walls \rightarrow t-type thermocouples
- Concentration —> FID (300 Hz)

- Different roughness conditions at walls
- Different wall heating (DW, UW)
- Different **thermal fluxes** (different ΔT)

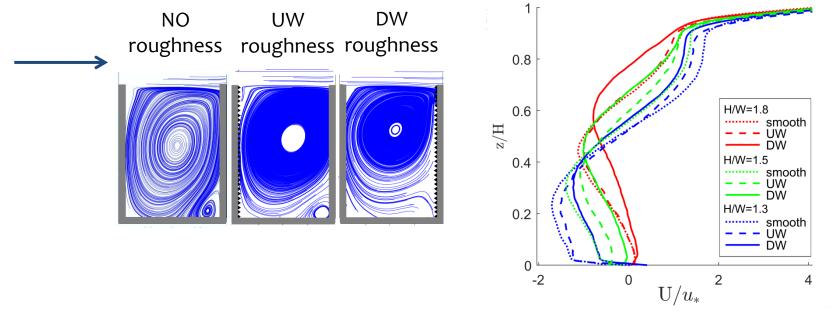
$$Fr_{i} = \frac{U}{\sqrt{gH\Delta T/T_{0}}} = \frac{inertia}{buoyancy} \qquad \qquad \Delta T \quad 0 K \quad 70 K \quad 170 K \quad 240 K \\ Fr_{i} \quad \infty \quad 0.62 \quad 0.40 \quad 0.34 \end{cases}$$

W

Effect of canyon geometry



Effect of wall roughness



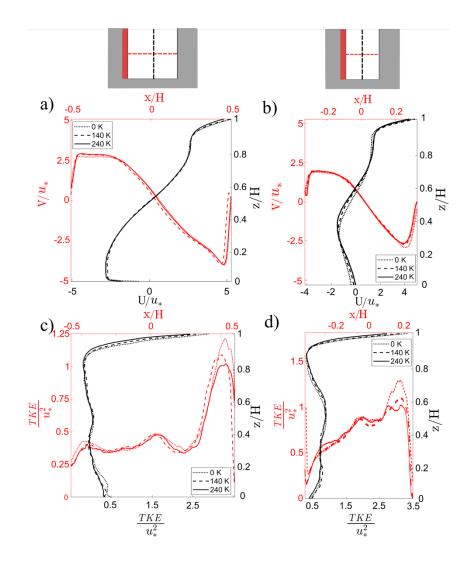
ROUGHNESS on downwind wall (DW) facilitates formation of 2nd cell

slow down of canyon ventilation

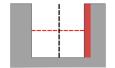
Effect of wall heating – upwind wall

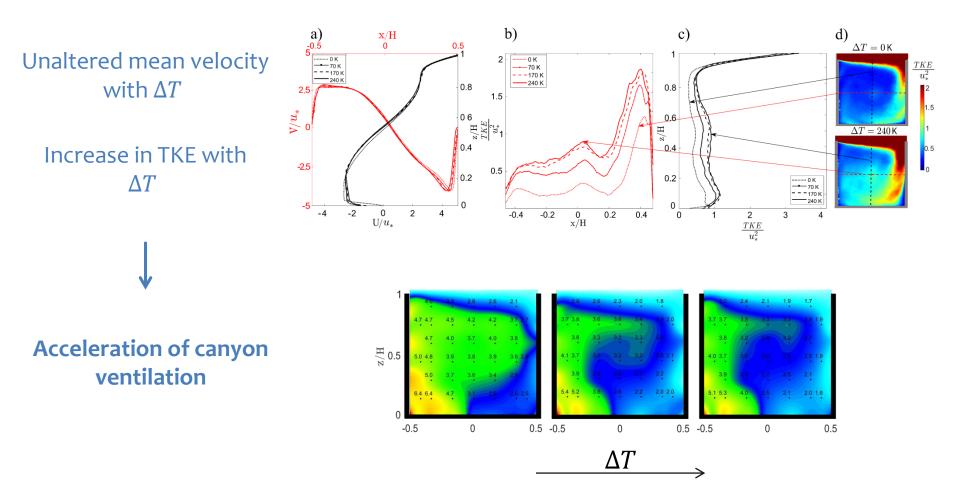
Unaltered mean velocity field with ΔT





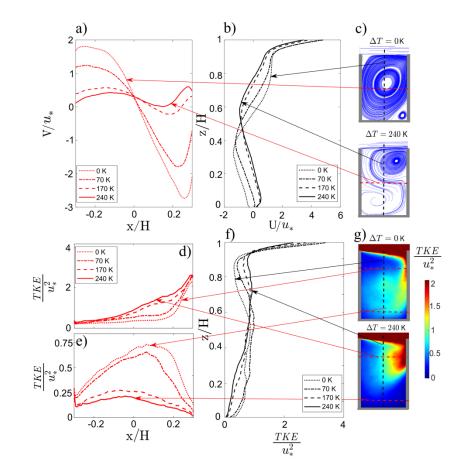
Effect of wall heating – downwind wall of a square cavity



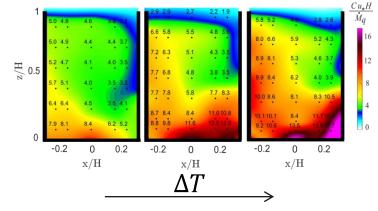


Effect of wall heating – downwind wall of a narrow cavity





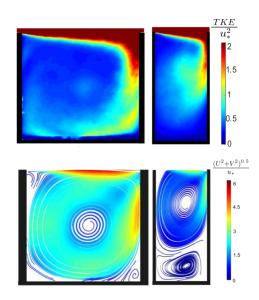
Formation of second cell ↓ Penetration of TKE at street level is inhibited ↓ Slow down of canyon ventilation

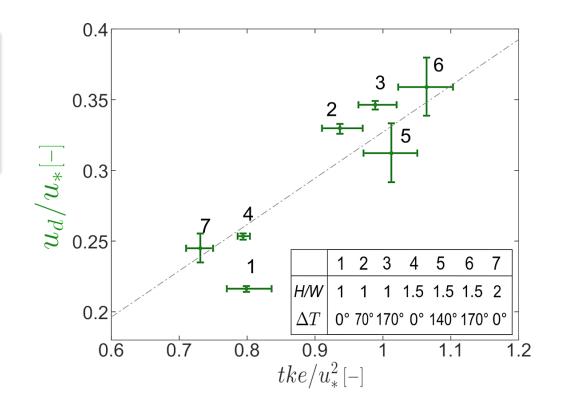




Turbulent kinetic energy and canyon ventilation

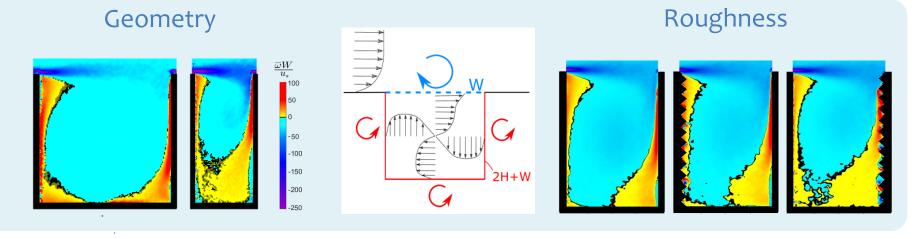
The vertical transport is governed by the Turbulent Kinetic Energy (TKE) field





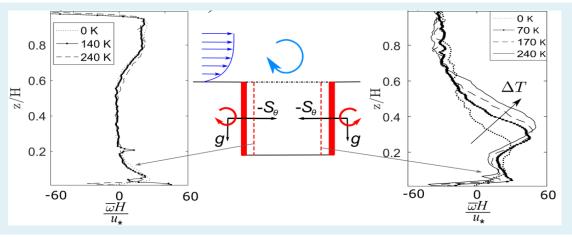
Vorticity balance interpretation

$$\frac{D\boldsymbol{\omega}}{Dt} = \boldsymbol{\omega} \cdot \nabla \mathbf{u} + \nu \nabla^2 \boldsymbol{\omega} - \mathbf{S}_{\mathbf{T}} \times \mathbf{g},$$



Heating

$$\mathbf{S_T} = \frac{1}{T} \nabla T.$$



Conclusions

The removal of pollutants depends on the topology of the mean velocity field and on the TKE inside the cavity

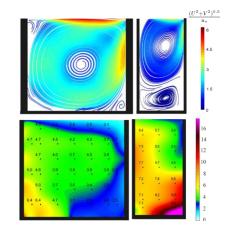
As H/W increases:

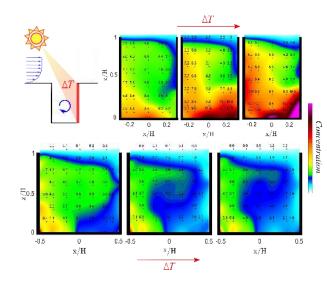
- Surplus of anticlockwise vorticity near the walls
- Formation of a 2nd second counter-rotating cell
- Slow down of removal of pollutant from the cavity

Adding roughness to the downwind wall facilitates the transition to two recirculating cells

Thermal fluxes at the upwind wall have negligible effects on both the mean and TKE fields

The heating of the downwind wall has opposite effects depending on the street aspect ratio





Bibliography

- Fellini, Ridolfi, Salizzoni, *Street canyon ventilation: combined effect of cross-section geometry and wall heating*, Quarterly Journal of the Royal Meteorological Society, 2020.
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- Salizzoni, Marro, Soulhac, Grosjean, and Perkins, *Turbulent transfer between street canyons* and the overlying atmospheric boundary layer. Boundary-Layer Meteorology, 2011.

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