

Hydrological and hydraulic models for determination of flood-prone and flood inundation areas

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Abstract. Geographic Information Systems (GIS) are widely used in most studies on water resources. Especially, when the topography and geomorphology of study area are considered, GIS can ease the work load. Detailed data should be used in this kind of studies. Because of, either the complication of the models or the requirement of highly detailed data, model outputs can be obtained fast only with a good optimization. The aim in this study, firstly, is to determine flood-prone areas in a watershed by using a hydrological model considering two wetness indexes; the topographical wetness index, and the SAGA (System for Automated Geoscientific Analyses) wetness index. The wetness indexes were obtained in the Quantum GIS (QGIS) software by using the Digital Elevation Model of the study area. Flood-prone areas are determined by considering the wetness index maps of the watershed. As the second stage of this study, a hydraulic model, HEC-RAS, was executed on the possible flood prone areas to determine flood inundation areas under different return period-flood events. River network cross-sections required for this study were derived from highly detailed digital elevation models by QGIS. Also river hydraulic parameters were used in the hydraulic model. Modelling technology used in this study is made of freely available open source softwares. Based on case studies performed on watersheds in Turkey, it is concluded that results of such studies can be used for taking precaution measures against life and monetary losses due to floods in urban areas particularly.

Keywords: Flood, wetness index, GIS, QGIS, DEM, HEC-RAS, Hydrologic model, Hydraulic model

1 Introduction

Floods are among the most common natural hazards that cause several damages to the properties, injuries and losses of lives. It occurs in different regions all over the World extending to more than 1/3 of the area and 82% of population (Dilley, 2005). Urbanization and continuous industrial activities trigger the flood and increase the flood damage in flood plains of hydrological watersheds. It is therefore very important to delineate flood-prone areas well in advance to be able to take preventive measures to minimize any damage the flood may cause.

Floods are studied by hydrological, hydraulic and topographical inputs to be analyzed at both spatial and temporal scales. For this aim, numerical models have been developed to calculate flood discharge due to precipitation of a given return period. With the help of the recent modelling technology, flood forecasting becomes more accurate and requires less time than before. Geographical Information Systems (GIS) contributes as an important and very useful tool in this type of hydrologic and hydraulic models.

In this study, a regional-scale hydrologic model was developed first for the delineation of the flood-prone areas in hydrological watersheds. Two topographical indexes were used in the hydrological model. Once flood prone areas are determined, a hydraulic model was implemented at local-scale, for calculating the flow depth and velocity in risky areas along the river for which the freely available HEC-RAS hydraulic model was used. Case study from a watershed in Northern part of Turkey shows the applicability of the models in delineating the flood-prone areas and the flow depth in risky parts of the river in terms of flood risk maps for given return periods of flood discharges.

2. Method

The proposed approach to assess flood hazard has a two-step process, the first step involves the detection and mapping of flood-prone areas by using GIS support and considering the topography of the watershed after which areas at risk are studied with more details by implementing the HEC-RAS hydraulic model to assess flooding parameters (Aksoy et al., 2014). This step is basically a flood susceptibility assessment process and is used to prioritize the flood-prone areas in terms of the importance of the assets at risk. The second step is in fact the flood hazard assessment stage, leading to results which can support decision makers regarding the selection of preventive measures. In the literature, no study exists dealing with the problem as in the way used here other than a case study performed very recently by Samela et al. (2015) for delineation of flood-prone areas in ungauged basins.

2.1. Regional scale hydrologic modelling by wetness indices

In the first step of regional-scale analysis that accommodates the hydrologic model, flood-prone areas in the watershed are identified. For this aim, two softwares, Quantum GIS (QGIS) and System for Automated Geoscientific Analyses GIS (SAGA GIS), fully supported by GIS were used. Both GIS softwares are freely available and user-friendly. The methods to map flood-prone areas at regional scale are based on the Topographic Wetness Index (*TWI*) approach and its variant, the *SAGA WI*, respectively.

TWI used in QGIS was suggested by Beven and Kirkby (1979) as

$$TWI = \ln\left(\frac{A_s}{\tan\beta}\right) \quad (1)$$

where A_s is the (upslope) flow accumulation area (or drainage area) per unit contour length (Wilson and Gallant, 2000) and β is the angle of the slope. *TWI* has found a wide range of application in hydrology (Moore et al., 1991; Quinn et al., 1995; Sorenson et al., 2005). Although *TWI* assumes that the soil in the watershed is homogeneous and isotropic as a constraint, it was found that topographical changes become much more important, therefore, the difficulty in this assumption becomes negligible compared to the change in the topography of the watershed. This allows one to use *TWI* in the hydrological analysis in this study.

The *SAGA WI* used in SAGAGIS is based on a modified catchment area calculation which does not consider the flow as a very thin film. As a result, it predicts, for cells situated in valley floors with a small vertical distance to a channel, a more realistic and with higher potential soil moisture as compared to *TWI*. This fact is translated to a wider area calculated as potentially covered with water during a flood event.

The *TWI* can be effectively used to reveal the flooding susceptibility by mapping the flood prone areas. The procedure to calculate the *TWI* and the *SAGA WI* in order to define the susceptibility to flooding (the flood-prone areas) is very straight forward since the selected open source software Quantum GIS (QGIS) incorporates the respective routines built into the SAGA GIS.

2.2. Local scale Hydraulic Modelling in HEC-RAS

The hydraulic analysis is performed to determine hydraulic characteristics of water flow, such as flow depth, flow velocity, forces due to water flowing on a surface or at a hydraulic structure, etc. The aim of this part in this study is to determine the characteristics of flow and potential flooding in streams and areas that have suffered flooding in the past taking into account the precipitation and surface runoff draining from the basin.

Hydraulic modelling and analysis have shown extensive research effort to simulate flood propagation in rivers. This is expressed by numerous 1- and 2-dimensional simulation models including HEC-RAS, Mike11, FLO-2D etc. The outcomes of these models, in riverine flood hazard assessment, include the level of inundation (flood water level), the intersection of the flood level with the terrain (ground surface) to create the flood plain extent, the difference between the flood level and the terrain, which is used to calculate the depth and the flow velocity.

Hydraulic analysis for assessing hydraulic behavior for the needs of this study was implemented with the HEC-RAS software (USACE, 2010) that can be downloaded from the official Hydrologic Engineering Center, River Analysis System (HEC-RAS) web site freely.

3. Study Area and Watershed

As mentioned previously, the pilot implementation of flood hazard assessment includes two phases: a regional implementation and a local implementation. The regional implementation was done in Ikizce watershed located in Samsun province, the Middle Black Sea region in northern part of Turkey (Figure 1). The local implementation for the flood hazard assessment was done for the Akçay Creek in the Ikizce watershed. Akçay Creek is located within the Terme district of Samsun, which is 56 km to the East of the Samsun city center. All rivers including the Akçay Creek are known to be critical in terms of flash floods, causing losses, even casualties in the watershed.

Samsun province exhibits the Northwestern climate of Turkey, which covers the coastal Black Sea area including the Northern faces of the mountains and Northeastern part of Marmara region. The mean annual precipitation in Samsun is 683.2 mm. Maximum precipitation is seen in October, November and December with the values of 88.8 mm, 82.5 mm and 72.9 mm, respectively. It may be of particular interest to mention that the maximum daily precipitation recorded in Samsun is 113.2 mm during 32 years of measurements. The temperature difference between summer and winter is not sparse. Summers are relatively cool whereas winters are relatively warmer in coastal lowlands and colder in higher ground with precipitation of snow. The mean annual temperature is 14.2 °C, with the mean monthly summer temperatures of 23.3 °C, 23.2 °C and 20.0 °C in August, July and June, respectively. In the winter, the mean monthly values drop down to 6.6 °C, 7.0 °C and 7.8 °C in February, January and March, respectively. Natural plant cover is humid and wide-leaved forest, turning to coniferous trees in higher lands. In the coastal areas along the river banks, there is an intense population of reeds. In the coastal region of

Samsun (including Terme) the major type of encountered soil is clayey sand. The mean infiltration capacity of this soil type is measured to be 9 mm/hr, a quite low value.

Akçay Creek discharges directly to Black Sea (Figure 1). The downstream region of the creek is generally covered by agricultural area, as well as industrial facilities. There is an LNG power plant, an ancient bridge and a primary school building in the close vicinity of this zone. The major intercity highway which connects Samsun to Ordu in the East passes across the Akçay Creek with a new bridge (Figure 2).



Figure 1. Geographic location and terrain view of Samsun (courtesy of GoogleEarth®) and Ikizce watershed



Figure 2. A detailed view of Akçay Creek in Ikizce watershed

4. Data

The data for the regional-scale implementation were compiled from the maps. The Ikizce watershed was delineated from the website of Ministry of Forestry and Water Affairs of Turkey <http://www.geodata.ormansu.gov.tr>. For the hydrological model, 1/25000 scale maps were used as the topographical data obtained from Turkish Army General Command of Mapping.

For the local-scale model, cross-sections of the river were produced from 1/500 scale digital maps. The 2, 5, 10, 25, 50, 100 and 500-year return period flood hydrographs of the Akçay Creek were obtained from State Hydraulic Works (DSI) of Turkey as given in Figure 3. Peak discharges of the flood hydrographs are tabulated in Table 1. A steady-state flow with the flood discharge is assumed in the hydraulic analysis. Cross sections at every 20 m longitudinal distance were used to define the flow geometry in HEC-RAS. These cross-sections were extracted from the DEM with a grid resolution of 2 m.

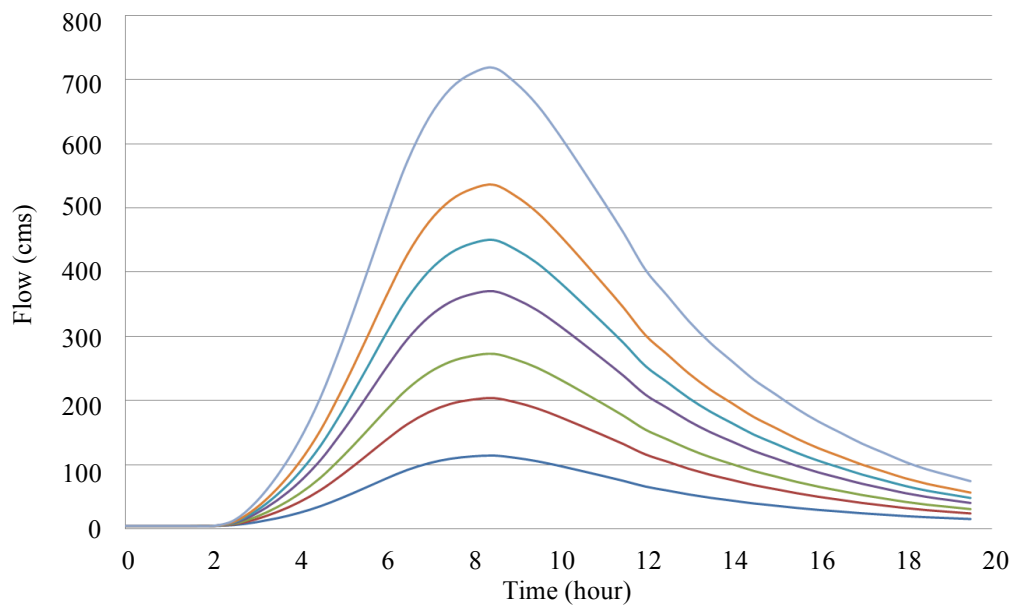


Figure 3. Flood hydrograph in Akçay Creek for 2, 5, 10, 25, 50, 100 and 500-year return periods

Table 1. The flood hydrograph of Akçay Creek

t (hour)	Q ₂	Q ₅	Q ₁₀	Q ₂₅	Q ₅₀	Q ₁₀₀	Q ₅₀₀
	(m ³ /s)						
6.50	109.57	199.02	267.87	365.30	445.09	531.01	713.10

5. Implementation

5.1. Regional-scale implementation

For the regional scale, the previously explained methodology was used which was implemented in the QGIS and SAGAGIS. For this purpose, the following procedure is applied:

- Using the sub-basin templates in <http://geodata.ormansu.gov.tr>, the DEM files are trimmed into sub-basins, such that each file covers a single sub-basin.

- Once the sub-basin DEMs are generated, they are processed with the integrated computational steps using QGIS interface.
- The aspects, unit catchment area, *TWI* and *SAGA WI* are calculated.
- These indexes are converted into maps which show the flood-prone areas as the result of regional-scale flood hazard assessment.

Although there is not a strict universal criterion to differentiate the flood-prone areas solely on the isolated values of the aforementioned indexes, the distribution of the indexes across the river basins give very crucial qualitative information about the flood susceptibility of any location of interest within the basin. Figures 4a and 4b shows the *TWI* and *SAGA WI* for the Akçay Creek in Ikizce basin. In Figure 4c, a close-up view of the *SAGA WI* is shown.

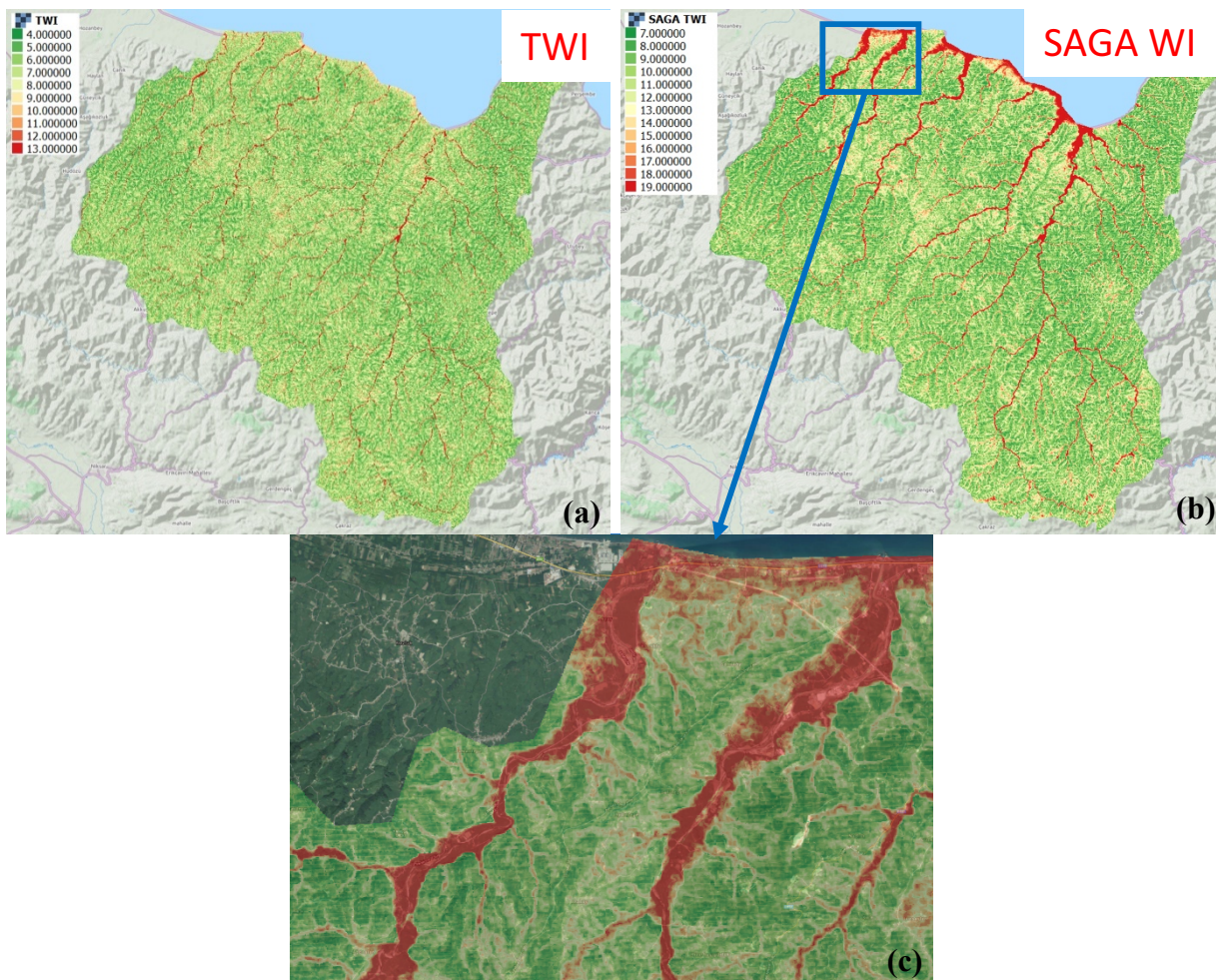


Figure 4. Regional-scale analysis of Ikizce watershed, (a) TWI, (b) SAGA WI; (c) a close-up view of downstream area of Akçay Creek

5.2. Local-scale implementation

The area chosen for the local scale flood hazard assessment is the Akçay Creek in the Akçay village, which is located in the border of Samsun and Ordu provinces. In the output of the regional scale flood hazard assessment model, the downstream area of Akçay Creek came out to be a critical flood-prone zone based on wetness indexes in Figures 4a and 4b. The close-up view of this location in Figure 4c shows that the downstream section of the

river is the most susceptible zone in the watershed against flooding. Therefore, it was decided to model this region at local scale by means of the 1-D hydraulic modelling using the HEC-RAS software.

As stated above, for the hydraulic analysis, cross-sections of the river were produced from 1/500 scale-digital maps at every 20 m along the river. The HEC-RAS model was run for the 2-, 5-, 10-, 25-, 50-, and 100-year return period flood hydrographs under steady-state subcritical flow conditions.

Results are given in Figure 5 for floods with the above mentioned return periods. As can be seen, when the peak discharge exceeds the 10 year-return period extreme value, the creek tends to overflow from its bed. This draws a parallel picture with what happens in reality. Especially at the last 300 m of the creek (i.e. downstream of the highway bridge, see Figure 2) the inundation area is considerably high. In the modelling, it was seen that the highway bridge is flooded with return periods higher than 100 years. A flood recorded in July 2012 was found to be roughly the 85 year-return period flood in the watershed (Onoz et al., 2012). If the storm surge that rises the sea level at the downstream (say, at the order of 0.5-1 m) is taken into account, the observation in July 2012 comes to an agreement with the model results.

6. Conclusions

Following conclusions can be drawn from the regional scale and local scale flood hazard assessment modelling studies implemented:

- The proposed regional scale methodology is simple, easy and inexpensive (free software and minimum amount of data requirement); yet it is very effective in terms of pinpointing the flood-prone locations in hydrological watersheds.
- 1/25000 scale maps are very convenient for the application of the regional model to yield high resolution results. However, experience shows that even the ASTER DEM maps (freely downloadable from <http://gdem.ersdac.jspacesystems.or.jp>) can yield satisfactory results on revealing flood-prone areas.
- An additional point, based on several case studies performed by Ermiş (2015) (not covered in this study), is that the regional scale flood hazard assessment model can be operated both with small basins (in size of a few hundred km²) and relatively large basins (in size of a few thousand km²). In any case, operating with smaller basins may be more practical since the precision of the results would be presumably higher.
- The local scale flood hazard assessment model (the 1-D hydraulic model) implemented by use of HEC-RAS yielded precise results for the probable flood inundation areas for different return periods of flood occurrences.
- As a specific result of the case study here, it was seen that the Akçay Creek overflows its bed for return periods larger than 10 years and the events tend to become more catastrophic for extreme events larger than 100 year-return period, since the highway bridge is inundated leading to further flooding upstream.

It should additionally be noted that any possible sea level rise in Black Sea (i.e. due to storm surge, wind or wave setup) was not accounted for in the flood modelling. Such rises in the sea level are likely to increase the flooded areas due to the downstream-controlled flow regime in the river.

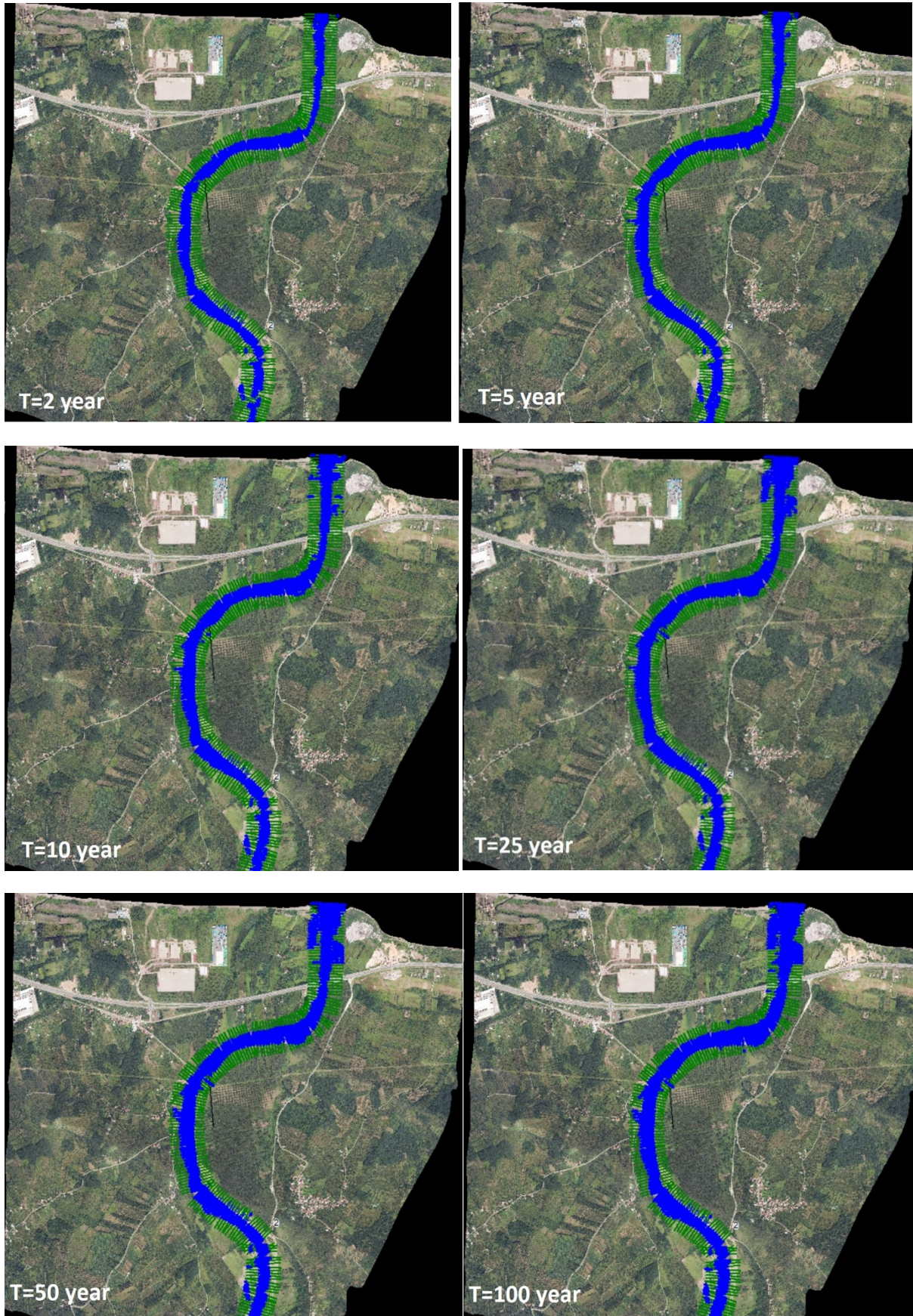


Figure 5. Results of local scale hydraulic model for different return period floods

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